

HILLSIDE SUBDIVISION PRELIMINARY STORMWATER MANAGEMENT REPORT

**318 Lake Street
Picton, ON
Prince Edward County**

May 2025



Table of Contents

1.0	INTRODUCTION	1
1.1	Project Background.....	1
1.2	Location and Site Description	1
1.3	Geotechnical Investigation.....	3
1.4	Design Criteria	3
2.0	STORM DRAINAGE.....	3
2.1	Existing Storm Drainage and Model Parameters	3
2.2	Pre-development Conditions	3
2.3	Proposed Conditions.....	4
2.4	Rainfall Distribution	5
2.5	Existing Drainage Summary	7
2.6	Proposed Storm Drainage Summary.....	7
2.6.1	Uncontrolled Drainage	7
2.6.2	Pond Inflows and Allowable Release Rates	7
3.0	STORMWATER MANAGEMENT	7
3.1	Water Quality	7
3.1.1	Permanent Pool Sizing	8
3.1.2	Extended Detention Quality Storage Sizing	8
3.2	Water Quantity	8
3.3	Groundwater Impacts.....	9
4.0	MAINTENANCE	10
5.0	TEMPORARY EROSION AND SEDIMENTATION CONTROLS	10
6.0	CONCLUSIONS	10

List of Figures

Figure 1 – Site Location Map
Figure 2 – Preliminary Site Plan
Figure 3 – Predevelopment Storm Drainage Area Plan
Figure 4 – Post Development Storm Drainage Area Plan

List of Appendices

Appendix A – Model Parameters
Appendix B – SWMHYMO Output
Appendix C – Quality Calculations
Appendix D – Maintenance Calculations

1.0 Introduction

1.1 Project Background

WSE Consulting Inc. has been retained as part of a consultant team to assist with Stormwater Management for the proposed development at 318 Lake Street.

1.2 Location and Site Description

The legal description of the property is located at 318 Lake St., Town of Picton, County of Prince Edward.

The property is bounded by County Road 10 to the west, County Road 22 to the south, and vacant land to the north and east.

There are existing homes and a business located adjacent to the site along County Rd 22 that are located at higher grade than the proposed developed portions of the site, as such there will be no impacts to these lands.

There is also an existing home located at 299 County Road 10 that will require the proposed development to develop a grading plan to ensure no adverse impacts either from draining to the existing property or receiving drainage from the property. This would be part of the grading design for final approval.

The site location is outlined on **Figure 1**. And the propose development outlined on **Figure 2**.

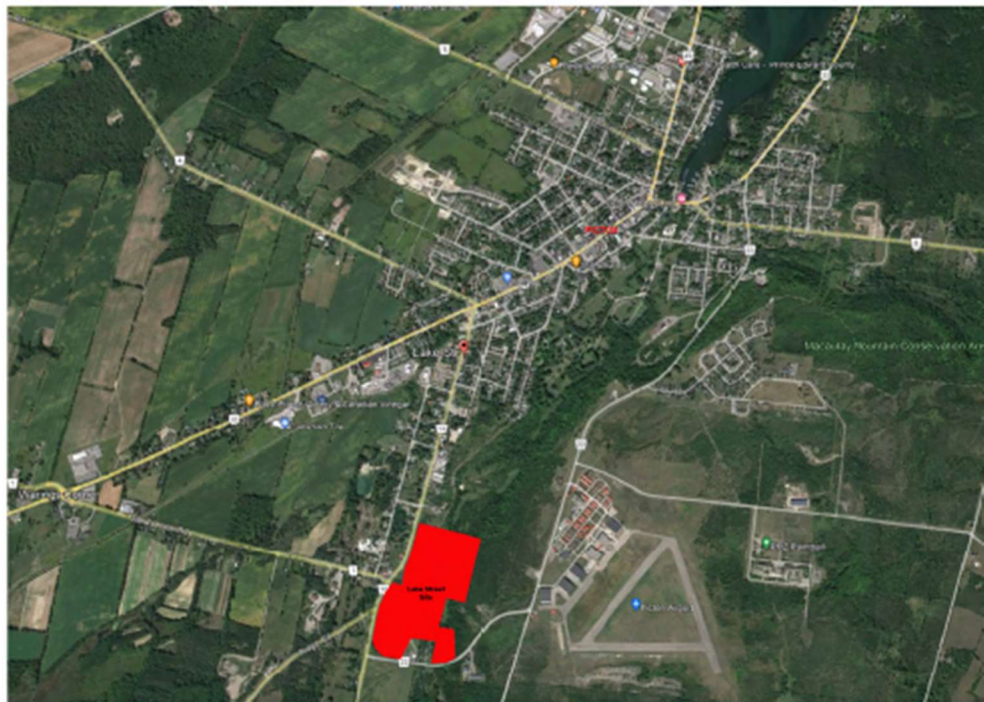


Figure 1 – Site Location

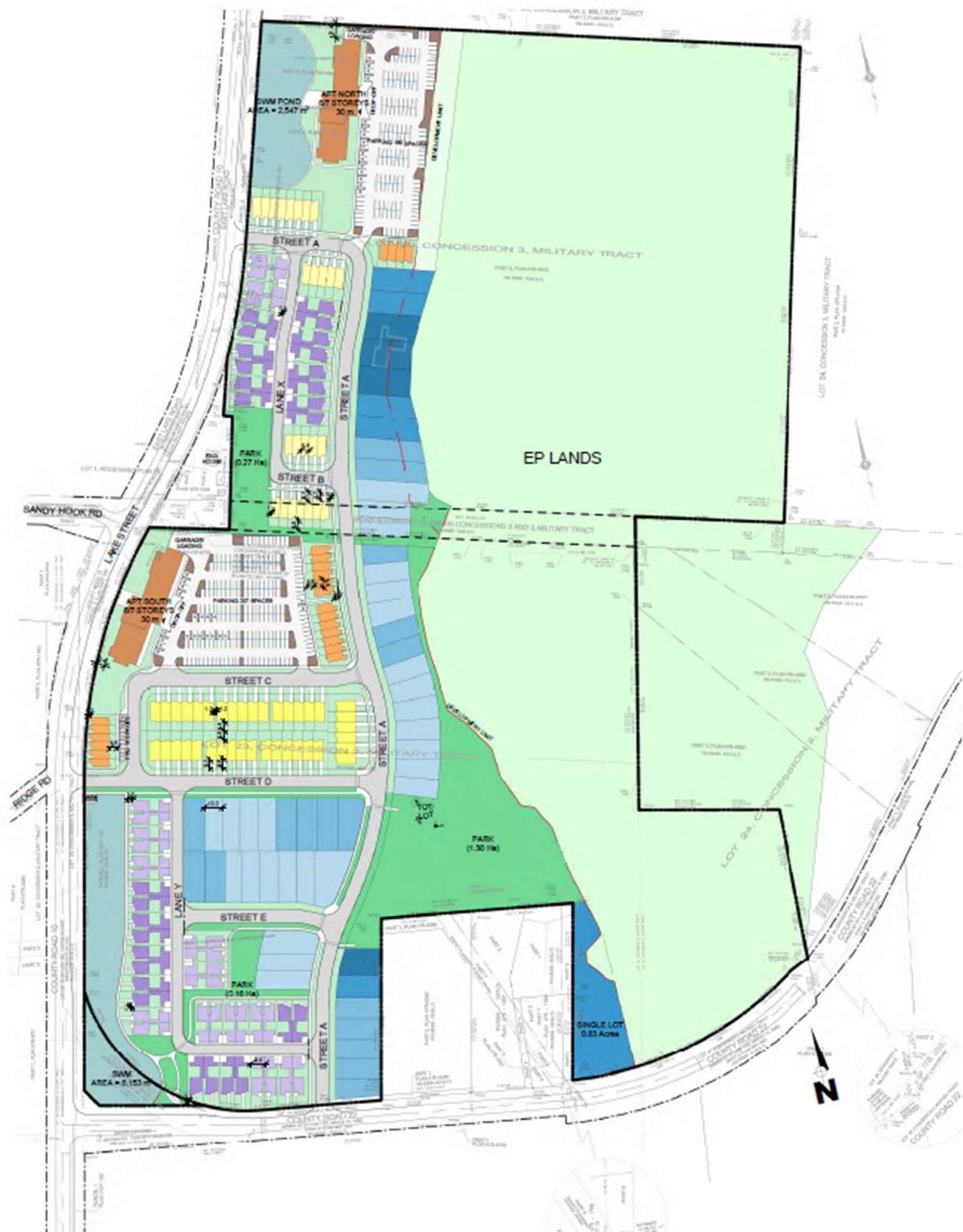


Figure 2 – Development Concept

1.3 Geotechnical Investigation

Geotechnical Investigation have been completed for the southern and northern portions of the project in 2 separate reports and have been referenced for soil conditions for the stormwater review. Excerpts from the reports are included in **Appendix A**.

The site soils generally consist of a surficial layer of topsoil, approximately 100 – 150 mm in depth. Underlying the topsoil ranges from a clay – silty clay – silt material.

The Ontario Ministry of Agriculture publishes a Soils Map for the County of Prince Edward. According to the Soils Map, there are three types of soils on the subject property. The site is predominantly covered by the 'Pontypool' series, described as a sand to sandy loam soil. There are small portions of 'Ameliasburgh' and 'Farmington' series as well. These are described as loam and sandy loam. This is generally consistent with the findings of the geotechnical report.

Soils have been assigned to Hydrologic Soils Group 'C', providing good drainage. Supporting information is included in **Appendix A**.

1.4 Design Criteria

Based on the size and function of the proposed development (Refer to Figure 2 for the Preliminary Site Plan), two (2) extended detention wet pond facilities have been selected as an appropriate best management practice for stormwater control. The Municipality will need to issue an Environmental Compliance Approval (CLI-ECA) for the facility. As such, design criteria have been considered based on the MECP Stormwater Management Planning and Design Manual (2003).

From these guidelines, the following design principles have been considered:

- Quantity control mitigation measures to ensure post development discharge rates do not exceed pre-development rates,
- Quality control mitigation measures to provide 'level 1', or enhanced, treatment of the 25mm quality rainfall event,

Water quantity and quality controls are thoroughly detailed in the MOE Design Manual for extended detention wet ponds.

2.0 STORM DRAINAGE

2.1 Existing Storm Drainage and Model Parameters

SWMHYMO Modeling software has been selected for modeling stormwater conditions. SWMHYMO generates rainfall hyetographs based on Intensity-Duration-Frequency (IDF) curve data that is inputted by the user. The Ministry of Transportation of Ontario (MTO) publishes IDF curve data for rainfall in the province. The MTO IDF curve data can be referred to in **Appendix 'A'** of this report.

2.2 Pre-development Conditions

The predevelopment site has been divided into five distinct sub-catchments; as outlined on the Predevelopment Storm Drainage Area Plan in **Figure 3**. For the purposes of this draft stormwater review only the internal catchments have been assessed to determine stormwater facility block sizing. The detailed report will evaluate external drainage for the purposes of conveyance and pond overflow requirements.

Under predevelopment conditions the area is undeveloped. The NASHYD watershed command is effective for modeling rural areas with high levels of infiltration. This command uses the Nash instantaneous unit hydrograph method to determine the outflow hydrograph and corresponding peak flow rates. The hydrograph is calculated based on a series of 'N' reservoirs. When $T_p = 0.67 T_c$, $N = 3$, and this is considered appropriate based on rainfall measurements in Ontario. Infiltration is calculated based on the SCS Curve Number (CN) method for loss. Selected composite CN values (MTO Drainage Management Manual), and time to peak calculations for each sub-catchment are included in Appendix A.

FIGURE #3
EXISTING
CATCHMENTS



2.3 Proposed Conditions

The post development site has been divided into 5 sub-catchment areas, similar to the pre-development area.

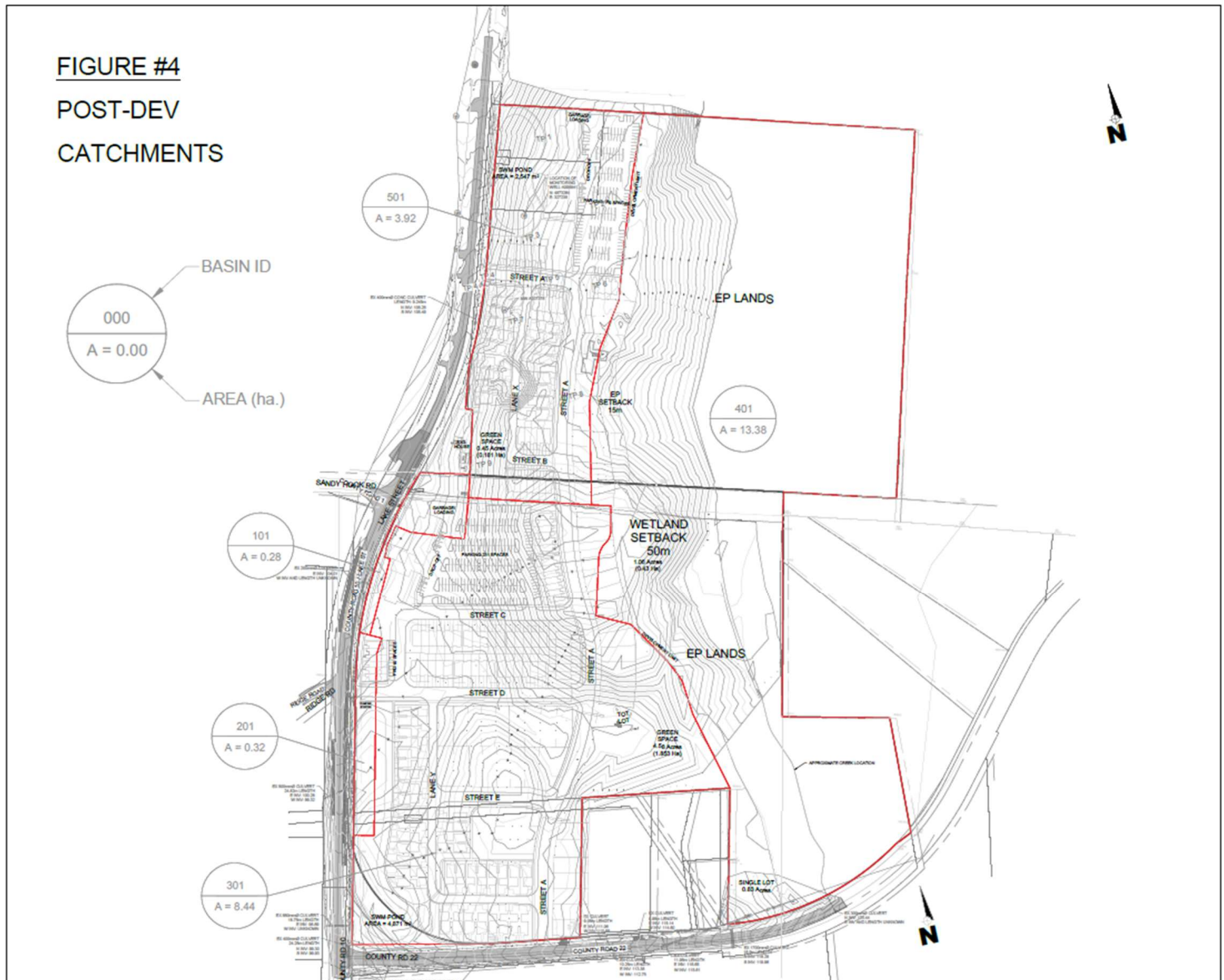
Areas that will undergo development have been assigned the STANDHYD command, which uses parallel instantaneous unit hydrographs for the impervious and pervious areas of the catchment to predict the resulting outflow hydrograph and peak flows. Infiltration is calculated based on the SCS Curve Number (CN) method for loss.

The basins have been assigned a conservative (higher than expected) % imperviousness for the preliminary pond sizing in support of draft plan approval. During detailed design the %imperviousness will be further refined. The following outlines the imperviousness assigned to each catchment;

- 101 – 60%
- 201 – 60%
- 301 – 55%
- 401 – 5%*
- 501 – 65%

**The imperviousness is reflected in the modelling with an increased CN as the NASHYD command does not have an input for imperviousness, and the STANDHYD command is not appropriate for flows less than 20%.*

Further reference to these catchments can be made from the Post Development Storm Drainage Area Plan, shown in **Figure 4**.



2.4 Rainfall Distribution

Several rainfall distributions have been evaluated to determine the representative storm to be used for pond sizing. The following distributions were considered.

- 1 hr Chicago
- 4 hr Chicago
- 6 hr SCS Type II
- 12 hr SCS Type II
- 12 hr AES (30%)

100 year pre-development and post development estimates were generated using SWMHYMO for all areas, and pond volume estimates generated to determine the distribution that generate the largest storage requirement for the 5 catchment areas. The following Tables summarizes the findings.

Table 1 – 100 Year Storage Review – ‘100’ areas

	Pre-Dev.	Post Dev.	Storage
Distribution	(cms)	(cms)	(ha.m)
1 hr Chicago	0.111	0.112	-
4 hr Chicago	0.149	0.122	-
6 hr SCS	0.123	0.034	-
12 hr SCS	0.139	0.036	-
12 hr AES	0.051	0.013	-

Table 2 – 100 Year Storage Review – ‘200’ areas

	Pre-Dev.	Post Dev.	Storage
Distribution	(cms)	(cms)	(ha.m)
1 hr Chicago	0.360	0.134	-
4 hr Chicago	0.478	0.143	-
6 hr SCS	0.455	0.039	-
12 hr SCS	0.523	0.041	-
12 hr AES	0.196	0.015	-

Table 3 – 100 Year Storage Review – ‘300’ areas

	Pre-Dev.	Post Dev.	Storage
Distribution	(cms)	(cms)	(ha.m)
1 hr Chicago	0.220	1.895	0.2619
4 hr Chicago	0.289	2.379	0.4374
6 hr SCS	0.191	0.977	0.5001
12 hr SCS	0.211	1.054	0.6467
12 hr AES	0.076	0.393	0.6467

Table 4 – 100 Year Storage Review – ‘400’ areas

	Pre-Dev.	Post Dev.	Storage
Distribution	(cms)	(cms)	(ha.m)
1 hr Chicago	0.516	0.509	-
4 hr Chicago	0.678	0.667	-
6 hr SCS	0.776	0.761	-
12 hr SCS	0.929	0.908	-
12 hr AES	0.395	0.387	-

Table 5 – 100 Year Storage Review – ‘500’ areas

	Pre-Dev.	Post Dev.	Storage
Distribution	(cms)	(cms)	(ha.m)
1 hr Chicago	0.162	1.141	0.1303
4 hr Chicago	0.217	1.265	0.2120
6 hr SCS	0.212	0.470	0.2428
12 hr SCS	0.248	0.504	0.3116
12 hr AES	0.092	0.187	0.3116

It can be seen in the above table that the 12 hr SCS and 12hr AES distributions generated the greatest storage requirement. However the AES generated lower pre-development rates, as such the 12 hr AES event has been selected as the representative distribution and the 2 year through 100 year rainfalls have been evaluated for the pre-development and post development conditions.

2.5 Existing Drainage Summary

The following table summarizes the SWMHYMO model peak flow rates for the 12hr AES distribution for each sub-catchment under each storm event. The model output can be referred to in Appendix 'B' of this report.

Table 6 - 12 hr AES Pre-Development Flows (m³/s)

Event	100	200	300	400	500
2 year	0.013	0.051	0.022	0.102	0.023
5 year	0.022	0.085	0.035	0.166	0.038
10 year	0.029	0.110	0.045	0.214	0.050
25 year	0.037	0.143	0.057	0.282	0.066
50 year	0.044	0.169	0.066	0.337	0.78
100 year	0.051	0.196	0.076	0.395	0.092

2.6 Proposed Storm Drainage Summary

2.6.1 Uncontrolled Drainage

Areas 101, 201, and 401 represent the developed portion of the site that cannot be controlled at the ponds due to grading constraints. Flows from 101, and 201 will discharge to the municipal ditching on County Rd 10 prior to reaching the existing culverts, and flows from 401 will drain to the existing creek. As outlined in section 2.4 the post development flows are expected to be less than the pre-development rates for all distributions, as such no stormwater quantity mitigation is required for these portions of the development.

2.6.2 Pond Inflows and Allowable Release Rates

Area 301, and 501 represent the developed site areas that will ultimately outlet to the proposed stormwater management ponds. Stormwater quantity controls for design of the ponds are discussed in Section 3.2 below.

3.0 STORMWATER MANAGEMENT

3.1 Water Quality

Water Quality objectives have been taken from the Bay of Quinte RAP which indicates the required level of protection as 'Enhanced'. Enhanced protection corresponds to the end-of-pipe storage volumes required for the long-term average annual removal of 80% of suspended solids.

Table 3.2 of the Manual summarizes the volumetric water quality storage requirements, an excerpt of which has been provided below:

Protection Level	SWMP Type	Storage Volume (m ³ /ha) for Impervious Level			
		35%	55%	70%	85%
Enhanced 80% long-term S.S. removal	Infiltration	25	30	35	40
	Wetlands	80	105	120	140
	Hybrid Wet Pond/ Wetland	110	150	175	195
	Wet Pond	140	190	225	250

Area 301 will contribute to the stormwater pond to the south, while 501 will drain to the northern pond.

The total contributing area to the southern pond is 8.44 hectares, with an estimated imperviousness of 55%. Applying the storage volume requirement of 190 m³/ha results in a total water quality storage volume of 1,613.6 m³. Of this, 40 m³/ha is extended detention. The water quality volume is therefore comprised of 337.6 m³ for extended detention storage and 1,266 m³ for permanent pool storage.

The total contributing area to the northern pond is 3.92 hectares, with an estimated imperviousness of 65%. Applying the storage volume requirement of 213.3 m³/ha results in a total water quality storage volume of 836.1 m³. Of this, 40 m³/ha is extended detention. The water quality volume is therefore comprised of 156.8 m³ for extended detention storage and 679.3 m³ for permanent pool storage.

Area 101 will include some road areas and should be reviewed during detailed design to determine if an oil grit unit should be implemented.

Area 201 is expected to consist of only rooftop and rear yard runoff and as such would be relatively clean and would not require any quality treatment.

Area 501 will consist of only residential rooftop and rear yard runoff and as such would be relatively clean and would not require any quality treatment.

3.1.1 Permanent Pool Sizing

In following the MOE Design Manual, equations 4.5, 4.6. and 4.7, the forbay sizing for each pond has been determined as follows;

- Pond 301 : minimum length of 9.04m, a bottom width of 1.13m, and a depth of 1.0m
- Pond 501 : minimum length of 6.53m, a bottom width of 0.82m, and a depth of 1.0m

Appendix 'C' provides the calculations.

To prevent seepage of stormwater from the permanent pools or groundwater interception, a liner will need to be installed along each pond bottom, extending to above the height of the extended detention quality depth.

3.1.2 Extended Detention Quality Storage Sizing

Utilizing a stage-storage-discharge (SSD) relationship and the Route Reservoir command in SWMHYMO a 24hr draw down volume of 939.1m³ has been estimated for Pond 301, and 476.4 m³ for Pond 501. These exceed the volume recommended by Table 3.2 of the MOE manual and therefore governs.

A depth of 0.3m, controlled with a 100mm orifice is required to achieve the target 0.012m³/s 24hr draw down for Pond 301, and a depth of 0.3m, controlled with a 75 mm orifice is required to achieve the target 0.006 m³/s 24hr draw down for Pond 501.

Refer to Appendix 'B' for the stage-storage-discharge relationships.

3.2 Water Quantity

The ROUTERESERVOIR command was used to model the proposed ponding scenario (SSD) for all storms ranging from the 2-year up to and including the 100-year AES event. Table 3 and 4 below summarizes the uncontrolled runoff from Area 301 and Area 501, pond release rates, and post development outflows for storm events ranging from the 2-year up to and including the 100-year storm from the 2 proposed ponds.

Table 7 – Post Development Flows (m³/s) – Pond 301

	Pre-Dev	Post - uncontrolled	Post Controlled	Storage required
2 year	0.022	0.137	0.038	1762
5 year	0.035	0.203	0.050	2580
10 year	0.045	0.248	0.057	3159
25 year	0.057	0.304	0.065	3908
50 year	0.066	0.348	0.070	4496
100 year	0.076	0.393	0.075	5113

The outlet for the quantity events will be controlled by a combination of the quality orifice (100mm) and a quantity orifice (140mm). The total storage volume required is 5,113m³ at a total active depth of 1.7m.

An overflow weir and 0.3m freeboard has been sized at a width of 8.5m.

Table 8 – Post Development Flows (m³/s) – Pond 501

	Pre-Dev	Post - uncontrolled	Post Controlled	Storage required
2 year	0.023	0.068	0.041	666.5
5 year	0.038	0.099	0.057	867.1
10 year	0.050	0.120	0.067	1056
25 year	0.066	0.146	0.078	1285
50 year	0.078	0.167	0.085	1471
100 year	0.092	0.187	0.093	1669

The outlet for the quantity events will be controlled by a combination of the quality orifice (75mm) and a quantity orifice (207mm). The total storage volume required is 1669m³ at a total active depth of 1.2m.

An overflow weir and 0.3m freeboard has been sized at a width of 4.2m.

The preliminary modelling for both facilities is showing the discharge in the 2 year to 50 year events will exceed predevelopment flows. Further assessment is required at detailed design to refine the modelling and final pond geometry and outlet control.

Refer to Appendix 'B' for the stage-storage-discharge relationship that was generated for the pond.

3.3 Groundwater Impacts

Per QC's SWM manual (section 1.1.8) a review of groundwater impacts is required to ensure a facility does not create adverse impacts. As outlined in Section 3.1.1 a clay liner is recommended in the permanent pool portion of the ponds to prevent both seepage from the pond into the groundwater and interception of the groundwater table.

Additionally, it is recommended that through detailed design and construction LID measures be implemented as best possible to provide opportunities for surface runoff to be infiltrated into the groundwater regime. The follow measures are to be implemented in the detailed grading plan;

- Roof top leaders to pervious surfaces
- Reduced lot grading, where feasible
- Vegetated side yard and rear yard swales
- Major conveyance swales to be enhanced – with flat bottoms and check dams

Some of the above mentioned measures may require additional design justification during detailed design of the development.

4.0 Maintenance

Based on the annual loading rates provided in the MOE manual it has been estimated that both ponds forebays will require cleanout on a minimum 10 year cycle and the main cells should have a clean out on a minimum 20 year cycle.

The permanent pool portions of the forebay and main pond were sized with consideration for the loss of storage volume based on accumulated sediment.

Supporting calculations are provided in Appendix D.

A O&M manual should be provided prior to request for Municipal assumption.

5.0 Temporary Erosion and Sedimentation Controls

An erosion and sediment control strategy will be implemented as per the plan included in the drawing package in order to minimize the transfer of silt off site during construction. The following measures should be incorporated into the strategy as required:

- Environmental fencing and straw bales
- Regular inspection of the erosion and sediment control devices
- Removal & disposal of the erosion and sediment control devices after the site has been stabilized
- Removal of sediment from pond prior to request for municipal assumption
- All exposed earth to be re-vegetated

6.0 Conclusions

- Quality control is provided in two (2) wet pond facilities that will achieve a level 1 (enhanced) treatment.
- Quantity control is required in the facilities to control discharge from the ponds to ensure the total discharge from the development limits is maintained to pre-development levels.
- Silt fencing and straw bale barriers will be in place during construction.
- The forebays will require removal of accumulated sediment on a 10 year cycle and the main cells should have a cleanout on a minimum 20 year cycle.

Respectfully Submitted,



Adam Wilson, P.Eng
WSE Consulting Inc.

Active coordinate

43° 59' 15" N, 77° 9' 15" W (43.987500,-77.154167)

Retrieved: Tue, 29 Aug 2023 12:30:28 GMT



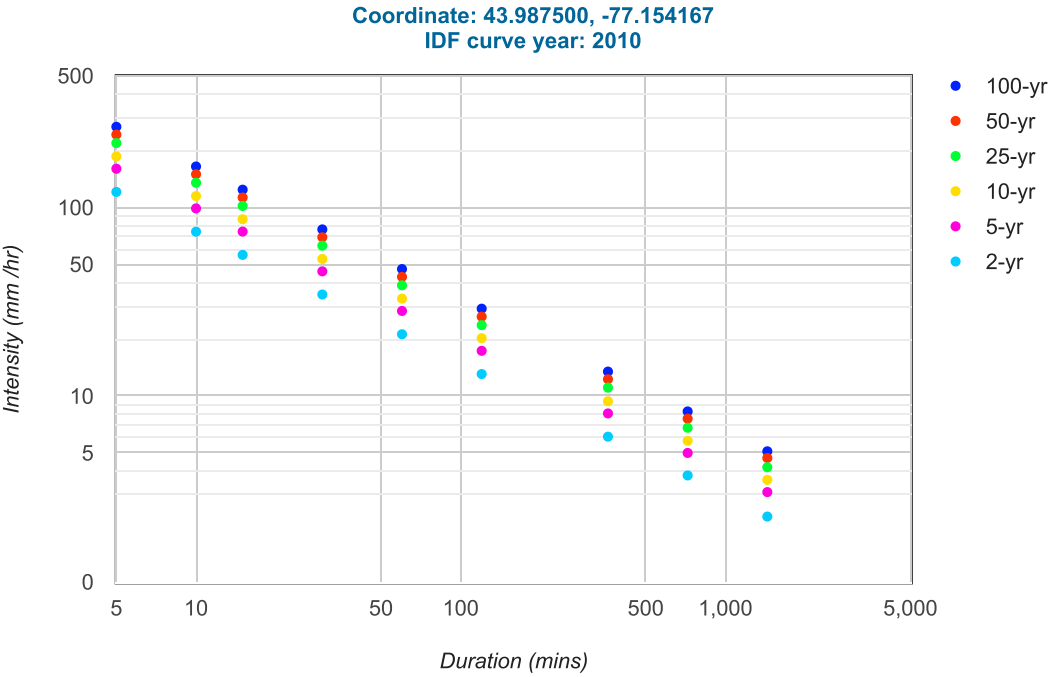
Location summary

These are the locations in the selection.

IDF Curve: 43° 59' 15" N, 77° 9' 15" W (43.987500,-77.154167)

Results

An IDF curve was found.



Coefficient summary

IDF Curve: 43° 59' 15" N, 77° 9' 15" W (43.987500,-77.154167)

Retrieved: Tue, 29 Aug 2023 12:30:28 GMT

Data year: 2010

IDF curve year: 2010

Return period	2-yr	5-yr	10-yr	25-yr	50-yr	100-yr
A	21.3	28.3	32.9	38.7	42.9	47.2
B	-0.699	-0.699	-0.699	-0.699	-0.699	-0.699

Statistics

Rainfall intensity (mm hr⁻¹)

Duration	5-min	10-min	15-min	30-min	1-hr	2-hr	6-hr	12-hr	24-hr
2-yr	121.0	74.5	56.1	34.6	21.3	13.1	6.1	3.8	2.3
5-yr	160.7	99.0	74.6	45.9	28.3	17.4	8.1	5.0	3.1
10-yr	186.9	115.1	86.7	53.4	32.9	20.3	9.4	5.8	3.6
25-yr	219.8	135.4	102.0	62.8	38.7	23.8	11.1	6.8	4.2
50-yr	243.7	150.1	113.1	69.6	42.9	26.4	12.3	7.6	4.7
100-yr	268.1	165.1	124.4	76.6	47.2	29.1	13.5	8.3	5.1

Rainfall depth (mm)

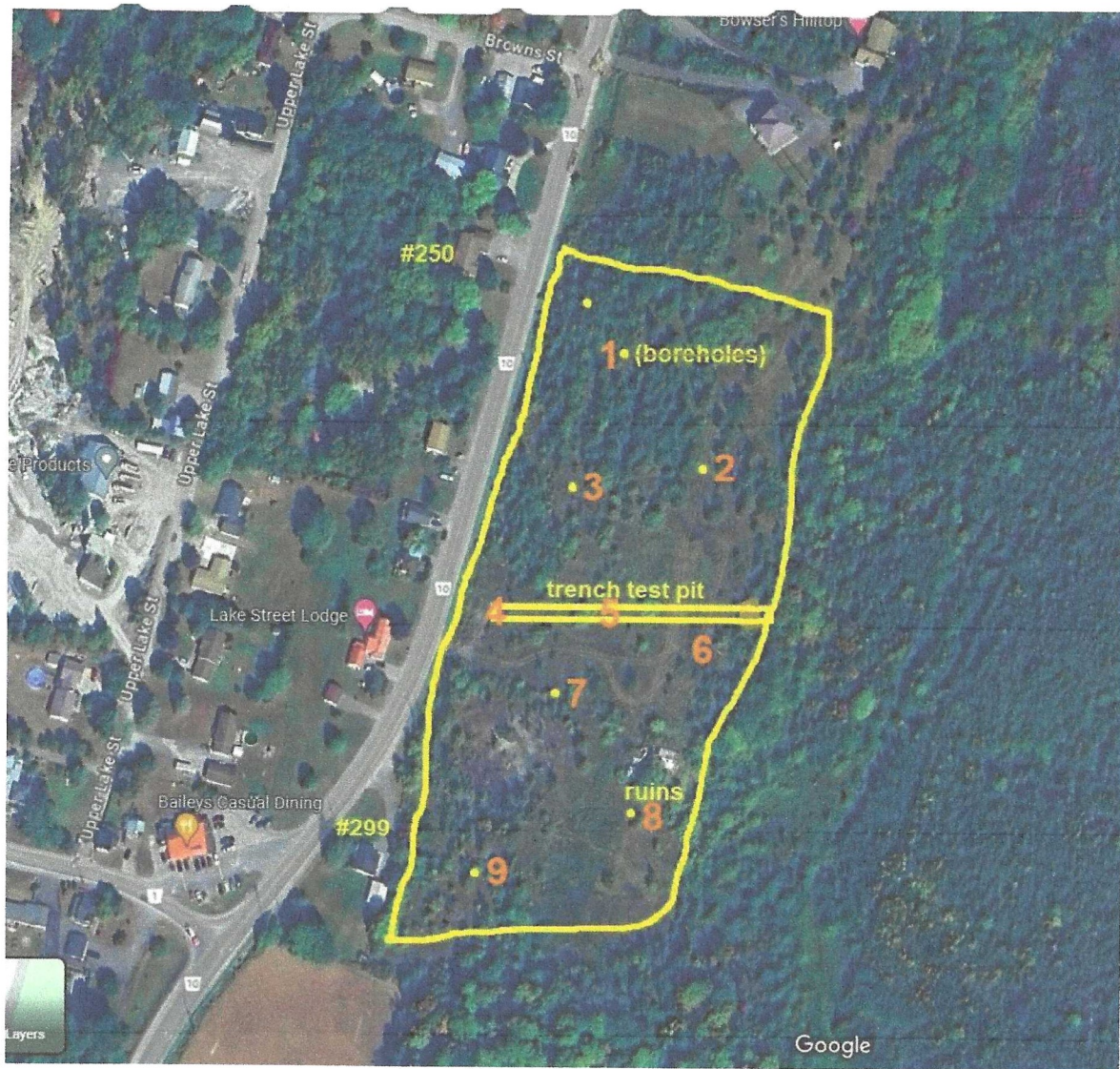
Duration	5-min	10-min	15-min	30-min	1-hr	2-hr	6-hr	12-hr	24-hr
2-yr	10.1	12.4	14.0	17.3	21.3	26.2	36.5	45.0	55.4
5-yr	13.4	16.5	18.6	23.0	28.3	34.9	48.5	59.8	73.7
10-yr	15.6	19.2	21.7	26.7	32.9	40.5	56.4	69.5	85.6
25-yr	18.3	22.6	25.5	31.4	38.7	47.7	66.4	81.8	100.7
50-yr	20.3	25.0	28.3	34.8	42.9	52.9	73.6	90.6	111.7
100-yr	22.3	27.5	31.1	38.3	47.2	58.2	80.9	99.7	122.9

Terms of Use

You agree to the [Terms of Use](#) of this site by reviewing, using, or interpreting these data.

[Ontario Ministry of Transportation](#) | [Terms and Conditions](#) | [About](#)

Last Modified: September 2016



Google Overhead Photo of Site

Soil Log

PROJECT: 287 Lake Street, Picton

Project No. 23-3-6593

DATE: May 29, 2024

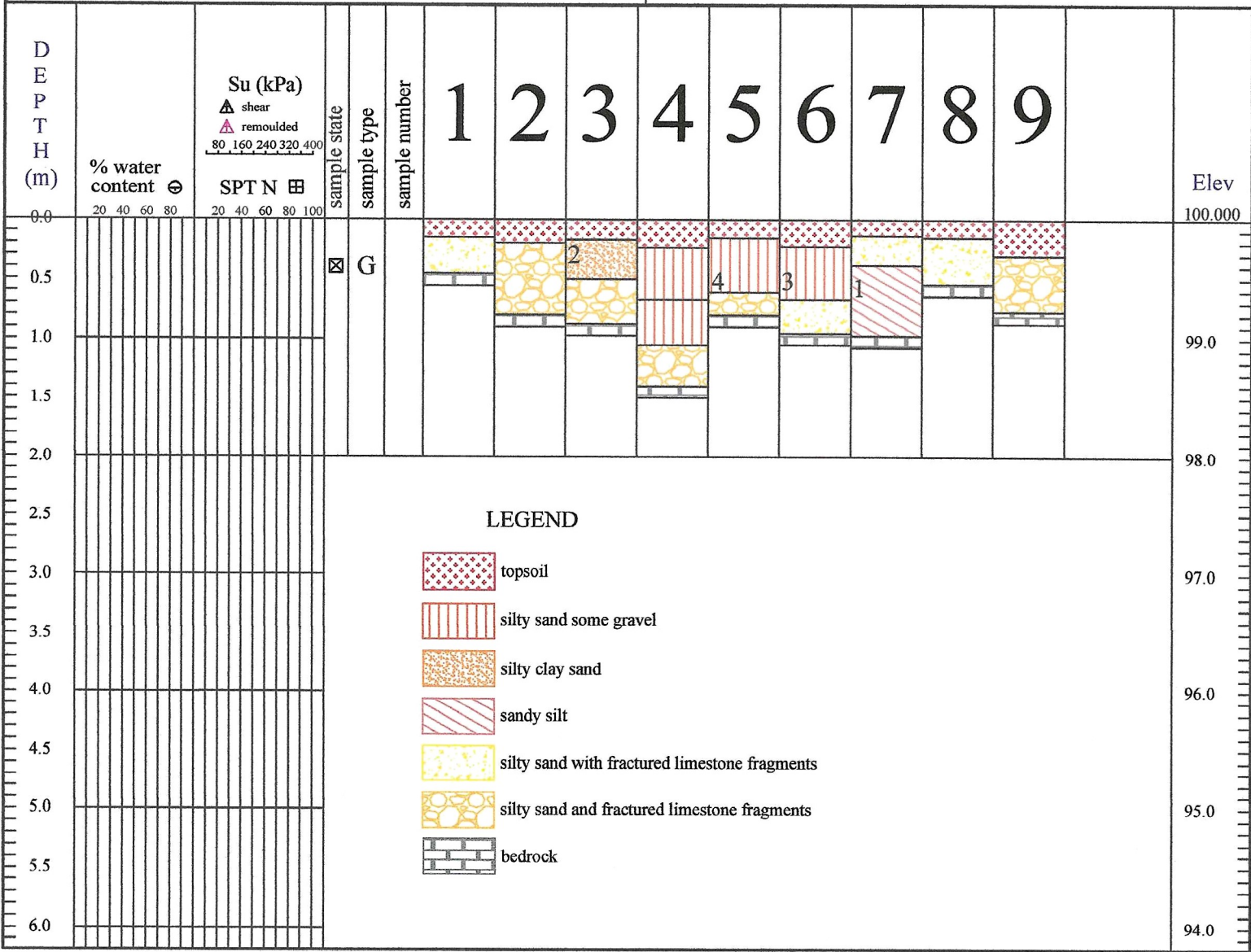
Sample Type A: auger S: spoon

Sample State ☒ remoulded ☐ intact

Test Hole Data

METHOD: Excavation

▼ encountered water elevation



Design Chart 1.08: Hydrologic Soil Groups (Continued)**- Based on Soil Texture**

<u>Sands, Sandy Loams and Gravels</u>	
- overlying sand, gravel or limestone bedrock, very well drained	A
- ditto, imperfectly drained	AB
- shallow, overlying Precambrian bedrock or clay subsoil	B
<u>Medium to Coarse Loams</u>	
- overlying sand, gravel or limestone, well drained	AB
- shallow, overlying Precambrian bedrock or clay subsoil	B
<u>Medium Textured Loams</u>	
- shallow, overlying limestone bedrock	B
- overlying medium textured subsoil	BC
<u>Silt Loams, Some Loams</u>	
- with good internal drainage	BC
- with slow internal drainage and good external drainage	C
<u>Clays, Clay Loams, Silty Clay Loams</u>	
- with good internal drainage	C
- with imperfect or poor external drainage	C
- with slow internal drainage and good external drainage	D

Source: U.S. Department of Agriculture (1972)

Design Chart 1.09: Soil Conservation Service Curve Numbers (Continued)

Land Use or Surface	Hydrologic Soil Group						
	A	AB	B	BC	C	CD	D
Fallow (special cases only)	77	82	86	89	91	93	94
Crop and other improved land	66** (62)	70** (68)	74	78	82	84	86 AMC I
Pasture & other unimproved land	58* (38)	62* (51)	65	71	76	79	81
Woodlots and forest	50* (30)	54* (44)	58	65	71	74	77
Impervious areas (paved)							98
Bare bedrock draining directly to stream by surface flow							98
Bare bedrock draining indirectly to stream as groundwater (usual case)							70
Lakes and wetlands							50

Notes

- (i) All values are based on AMC II except those marked by * (AMC III) or ** (mean of AMC II and AMC III).
- (ii) Values in brackets are AMC II and are to be used only for special cases.
- (iii) Table is not applicable to frozen soils or to periods in which snowmelt contributes to runoff.

Design Chart 1.07: Runoff Coefficients (Continued)**- Rural**

Land Use & Topography ³	Soil Texture		
	Open Sand Loam	Loam or Silt Loam	Clay Loam or Clay
CULTIVATED			
Flat 0 - 5% Slopes	0.22	0.35	0.55
Rolling 5 - 10% Slopes	0.30	0.45	0.60
Hilly 10- 30% Slopes	0.40	0.65	0.70
PASTURE			
Flat 0 - 5% Slopes	0.10	0.28	0.40
Rolling 5 - 10% Slopes	0.15	0.35	0.45
Hilly 10- 30% Slopes	0.22	0.40	0.55
WOODLAND OR CUTOVER			
Flat 0 - 5% Slopes	0.08	0.25	0.35
Rolling 5 - 10% Slopes	0.12	0.30	0.42
Hilly 10- 30% Slopes	0.18	0.35	0.52
BARE ROCK	COVERAGE³		
	30%	50%	70%
Flat 0 - 5% Slopes	0.40	0.55	0.75
Rolling 5 - 10% Slopes	0.50	0.65	0.80
Hilly 10- 30% Slopes	0.55	0.70	0.85
LAKES AND WETLANDS	0.05		

0.53

0.36.

² Terrain Slopes³ Interpolate for other values of % imperviousness

Sources: American Society of Civil Engineers - ASCE (1960)
 U.S. Department of Agriculture (1972)

Time to Peak Calculation**100**

RC 0.445 (50% @ 0.36, 50% @ 0.53)
CN 76.5 (50% @ 71, 50% @ 82)
length 260 m
0.26 km
width - m
slope 5.7 %
area 1.46 ha
0.0146 sq. km

Airport Method $tc=[3.26(1.1-RC)*L^{0.5}]/[s^{0.333}]$

tc= 19.2859 min 0.32143 hr

tp= 11.5715 min 0.19286 hr

200

RC 0.445 (50% @ 0.36, 50% @ 0.53)
CN 76.5 (50% @ 71, 50% @ 82)
length 320 m
0.32 km
width - m
slope 3.1 %
area 5.74 ha
0.0574 sq. km

Airport Method $tc=[3.26(1.1-RC)*L^{0.5}]/[s^{0.333}]$

tc= 26.2066 min 0.43678 hr

tp= 15.724 min 0.26207 hr

300

RC 0.53
CN 82
length 190 m
0.19 km
width - m
slope 6.3 %
area 1.89 ha
0.0189 sq. km

Airport Method $tc=[3.26(1.1-RC)*L^{0.5}]/[s^{0.333}]$

tc= 13.8768 min 0.23128 hr

tp= 8.32607 min 0.13877 hr

400

RC 0.36
CN 71
length 685 m
0.685 km
width - m
slope 2.77 %
area 13.97 ha
0.1397 sq. km

Airport Method $tc=[3.26(1.1-RC)*L^{0.5}]/[s^{0.333}]$

tc= 44.9727 min 0.74954 hr

tp= 26.9836 min 0.44973 hr

500

RC 0.36
CN 71
length 365 m
0.365 km
width - m
slope 5.8 %
area 3.11 ha
0.0311 sq. km

Airport Method $tc=[3.26(1.1-RC)*L^{0.5}]/[s^{0.333}]$

tc= 25.6669 min 0.42778 hr

tp= 15.4002 min 0.25667 hr


```
SSSSS W W M M H H Y Y M M OOO 999 999 -----
S W W W M M M H H H Y Y M M M O O 9 9 9 9
SSSSS W W W M M M H H H H Y Y M M M O O ## 9 9 9 9 Ver. 4.02
S W W M M M H H Y Y M M O O 9999 9999 July 1999
SSSSS W W M M M H H Y Y M M OOO 9 9 9 -----
StormWater Management Hydrologic Model 999 999 -----
```

```
*****
***** SWMHYMO-99 Ver/4.02 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTTHYMO-83 and OTTHYMO-89. *****
*****
***** ***** PROGRAM ARRAY DIMENSIONS ***** *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 15000 *****
***** Max. number of flow points : 15000 *****
*****
```

```
***** DETAILED OUTPUT *****
*****
* Input filename: C:\SWMHYM-1\LAKEST-1\100year.dat *
* Output filename: C:\SWMHYM-1\LAKEST-1\100year.out *
* Summary filename: C:\SWMHYM-1\LAKEST-1\100year.sum *
* User comments: *
* 1: *
* 2: *
* 3: *
```

```
001:0001-----
*# Project Name: [Lake Street] Project Number: 2022
*# Date : 10-08-2022
*# Modeller : []
*# Company :
*# License # :
```

```
*****
| START | Project dir.: C:\SWMHYM-1\LAKEST-1\
| Rainfall dir.: C:\SWMHYM-1\LAKEST-1\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 0
*****
```

```
001:0002-----
*
* Existing Condition
*
*
* 100 year event = 1 hr Chicago
*
```

```
-----
| CHICAGO STORM | IDF curve parameters: A= 971.139
| Ptotal= 48.81 mm | B= 1.500
| C= .726
used in: INTENSITY = A / (t + B)^C
Duration of storm = 1.00 hrs
Storm time step = 2.00 min
Time to peak ratio = .33
-----
```

The CORRELATION coefficient is = .9996862

TIME (min)	ENTERED (mm/hr)	COMPUTED (mm/hr)
5.	268.10	249.52
10.	165.10	164.90
15.	124.40	126.88
30.	76.60	79.34
60.	47.20	48.82
120.	29.10	29.78
360.	13.50	13.49
720.	8.30	8.17
1440.	5.10	4.94

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.03	15.562	.30	121.721	.57	32.195	.83	17.704
.07	17.083	.33	391.100	.60	28.944	.87	16.846
.10	19.009	.37	155.358	.63	26.366	.90	16.081

.13	21.539	.40	89.546	.67	24.267	.93	15.393
.17	25.035	.43	64.172	.70	22.521	.97	14.770
.20	30.231	.47	50.663	.73	21.043	1.00	14.204
.23	38.904	.50	42.230	.77	19.774		
.27	56.826	.53	36.437	.80	18.672		

```
001:0003-----
*
* Area 100
*
| CALIB NASHVD | Area (ha)= 1.46 Curve Number (CN)=76.50
| 01:100 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res. (N)= 3.00
| U.H. Tp (hrs)= .192
Unit Hyd Qpeak (cms)= .290
PEAK FLOW (cms)= .111 (I)
TIME TO PEAK (hrs)= .600
RUNOFF VOLUME (mm)= 16.344
TOTAL RAINFALL (mm)= 48.806
RUNOFF COEFFICIENT = .335
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
001:0004-----
*
* Area 200
*
| CALIB NASHVD | Area (ha)= 5.75 Curve Number (CN)=76.50
| 02:200 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res. (N)= 3.00
| U.H. Tp (hrs)= .262
Unit Hyd Qpeak (cms)= .838
PEAK FLOW (cms)= .360 (I)
TIME TO PEAK (hrs)= .700
RUNOFF VOLUME (mm)= 16.344
TOTAL RAINFALL (mm)= 48.806
RUNOFF COEFFICIENT = .335
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
001:0005-----
*
* Area 300
*
| CALIB NASHVD | Area (ha)= 1.89 Curve Number (CN)=82.00
| 03:300 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res. (N)= 3.00
| U.H. Tp (hrs)= .139
Unit Hyd Qpeak (cms)= .519
PEAK FLOW (cms)= .220 (I)
TIME TO PEAK (hrs)= .500
RUNOFF VOLUME (mm)= 19.964
TOTAL RAINFALL (mm)= 48.806
RUNOFF COEFFICIENT = .409
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
001:0006-----
*
* Area 400
*
| CALIB NASHVD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res. (N)= 3.00
| U.H. Tp (hrs)= .450
Unit Hyd Qpeak (cms)= 1.199
PEAK FLOW (cms)= .516 (I)
TIME TO PEAK (hrs)= .967
RUNOFF VOLUME (mm)= 13.514
TOTAL RAINFALL (mm)= 48.806
RUNOFF COEFFICIENT = .277
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
001:0007-----
*
* Area 500
*
| CALIB NASHVD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res. (N)= 3.00
| U.H. Tp (hrs)= .257
```

```

=====
001:0009
*
* Area 100
*
-----
| CALIB NASHDY | Area (ha) = 1.46 | Curve Number (CN)=76.50
| 01:100 | DT= 2.00 | Ia (mm)= 4.000 | # of Linear Res.(N)= 3.00
| | U.H. Tp(hrs)= .192
|
Unit Hyd Qpeak (cms)= .290
PEAK FLOW (cms)= .149 (i)
TIME TO PEAK (hrs)= 1.567
=====

```

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0012-----
*
* Area 400
-----
| CALIB NASHVD | Area (ha)= 14.13 | Curve Number (CN)=71.00
| 04:400 DTM= 2.00 | Ia (mm)= 4.000 | # of Linear Res. (N)= 3.00
| | U.H. Tp (hrs)= .450
-----
Unit Hyd Qpeak (cms) = 1.199

PEAK FLOW (cms)= .678 (i)
TIME TO PEAK (hrs)= 1.933
RUNOFF VOLUME (mm)= 27.136
TOTAL RAINFALL (mm)= 72.334
RUNOFF COEFFICIENT = .375

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```
001:0014-----*
*
*
*
*
*
*
```

```
*
* 100 year - 6hr SCS Type II
*
-----
| READ STORM |      Filename: C:\SWHMYM-1\LAKEST-1\100SCS6
| Ptotal= 80.90 mm |      Comments: 100year SCS 6hr
-----
      TIME  RAIN |  TIME  RAIN |  TIME  RAIN |  TIME  RAIN
      hrs  mm/hr |  hrs  mm/hr |  hrs  mm/hr |  hrs  mm/hr
      -----
      1.00  5.259 |  3.00 50.563 |  5.00  4.045 |
      2.00  7.686 |  4.00 10.113 |  6.00  3.236 |
      -----

001:0015-----
*
*
*
* Area 100
*
-----
| CALIB NASHVD |  Area  (ha)=  1.46  Curve Number  (CN)=76.50
| 01:100  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .192
|-----|

Unit Hyd Qpeak  (cms)=  .290

PEAK FLOW      (cms)=  .123 (i)
TIME TO PEAK   (hrs)=  3.033
RUNOFF VOLUME  (mm)= 38.170
TOTAL RAINFALL (mm)= 80.900
RUNOFF COEFFICIENT =  .472

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----

001:0016-----
*
* Area 200
*
-----
| CALIB NASHVD |  Area  (ha)=  5.75  Curve Number  (CN)=76.50
| 02:200  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .262
|-----|

Unit Hyd Qpeak  (cms)=  .838

PEAK FLOW      (cms)=  .455 (i)
TIME TO PEAK   (hrs)=  3.067
RUNOFF VOLUME  (mm)= 38.171
TOTAL RAINFALL (mm)= 80.900
RUNOFF COEFFICIENT =  .472

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----

001:0017-----
*
* Area 300
*
-----
| CALIB NASHVD |  Area  (ha)=  1.89  Curve Number  (CN)=82.00
| 03:300  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .139
|-----|

Unit Hyd Qpeak  (cms)=  .519

PEAK FLOW      (cms)=  .191 (i)
TIME TO PEAK   (hrs)=  3.000
RUNOFF VOLUME  (mm)= 44.579
TOTAL RAINFALL (mm)= 80.900
RUNOFF COEFFICIENT =  .551

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----

001:0018-----
*
* Area 400
*
-----
| CALIB NASHVD |  Area  (ha)= 14.13  Curve Number  (CN)=71.00
| 04:400  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .450
|-----|

Unit Hyd Qpeak  (cms)=  1.199

PEAK FLOW      (cms)=  .776 (i)
TIME TO PEAK   (hrs)=  3.200
RUNOFF VOLUME  (mm)= 32.736
TOTAL RAINFALL (mm)= 80.900
RUNOFF COEFFICIENT =  .405

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
```

```
001:0019-----
*
* Area 500
*
-----
| CALIB NASHVD |  Area  (ha)=  3.11  Curve Number  (CN)=71.00
| 05:500  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .257
|-----|

Unit Hyd Qpeak  (cms)=  .462

PEAK FLOW      (cms)=  .212 (i)
TIME TO PEAK   (hrs)=  3.067
RUNOFF VOLUME  (mm)= 32.736
TOTAL RAINFALL (mm)= 80.900
RUNOFF COEFFICIENT =  .405

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----

001:0020-----
*
*
*
*
*
* 100 year - 12hr SCS Type II
*
-----
| READ STORM |      Filename: C:\SWHMYM-1\LAKEST-1\100SCS12
| Ptotal= 99.70 mm|      Comments: 100year SCS 12hr
-----
      TIME  RAIN |  TIME  RAIN |  TIME  RAIN |  TIME  RAIN
      hrs  mm/hr |  hrs  mm/hr |  hrs  mm/hr |  hrs  mm/hr
      -----
      1.00  2.493 |  4.00  4.486 |  7.00  9.970 | 10.00  3.490
      2.00  2.493 |  5.00  8.474 |  8.00  2.243 | 11.00  3.490
      3.00  3.988 |  6.00 52.343 |  9.00  2.243 | 12.00  3.988
      -----

001:0021-----
*
*
*
* Area 100
*
-----
| CALIB NASHVD |  Area  (ha)=  1.46  Curve Number  (CN)=76.50
| 01:100  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .192
|-----|

Unit Hyd Qpeak  (cms)=  .290

PEAK FLOW      (cms)=  .139 (i)
TIME TO PEAK   (hrs)=  6.033
RUNOFF VOLUME  (mm)= 52.718
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT =  .529

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----

001:0022-----
*
* Area 200
*
-----
| CALIB NASHVD |  Area  (ha)=  5.75  Curve Number  (CN)=76.50
| 02:200  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .262
|-----|

Unit Hyd Qpeak  (cms)=  .838

PEAK FLOW      (cms)=  .523 (i)
TIME TO PEAK   (hrs)=  6.033
RUNOFF VOLUME  (mm)= 52.718
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT =  .529

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----

001:0023-----
*
* Area 300
*
-----
| CALIB NASHVD |  Area  (ha)=  1.89  Curve Number  (CN)=82.00
| 03:300  DT= 2.00 |  Ia  (mm)=  4.000  # of Linear Res. (N)= 3.00
|-----|
|      U.H. Tp (hrs)=  .139
|-----|

Unit Hyd Qpeak  (cms)=  .519
```

```
PEAK FLOW      (cms)=    .211 (i)
TIME TO PEAK   (hrs)=     6.000
RUNOFF VOLUME  (mm)=    60.470
TOTAL RAINFALL (mm)=    99.700
RUNOFF COEFFICIENT =    .607

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0024-----
*
* Area 400
*
-----
| CALIB NASHVD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.199

PEAK FLOW      (cms)=    .929 (i)
TIME TO PEAK   (hrs)=     6.167
RUNOFF VOLUME  (mm)=    45.920
TOTAL RAINFALL (mm)=    99.700
RUNOFF COEFFICIENT =    .461

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0025-----
*
* Area 500
*
-----
| CALIB NASHVD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .257

Unit Hyd Qpeak (cms)= .462

PEAK FLOW      (cms)=    .248 (i)
TIME TO PEAK   (hrs)=     6.033
RUNOFF VOLUME  (mm)=    45.920
TOTAL RAINFALL (mm)=    99.700
RUNOFF COEFFICIENT =    .461

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0026-----
*
*
*
*
*
*
*
*
*
*
* 2 year - 12hr AES
*
-----
| READ STORM | Filename: C:\SWMMHYM-1\LAKEST-1\2AES12.stm
| Ptotal= 44.80 mm | Comments: 2 year AES 12hr

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 8.064 | 4.00 6.720 | 7.00 1.344 | 10.00 .000
2.00 9.408 | 5.00 6.272 | 8.00 .448 | 11.00 .000
3.00 8.960 | 6.00 3.584 | 9.00 .000 | 12.00 .000

-----
001:0027-----
*
*
*
* Area 100
*
-----
| CALIB NASHVD | Area (ha)= 1.46 Curve Number (CN)=76.50
| 01:100 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .192

Unit Hyd Qpeak (cms)= .290

PEAK FLOW      (cms)=    .013 (i)
TIME TO PEAK   (hrs)=     3.033
RUNOFF VOLUME  (mm)=    14.009
TOTAL RAINFALL (mm)=    44.800
RUNOFF COEFFICIENT =    .313

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0028-----
*
* Area 200
*
-----
```

```
*
-----
| CALIB NASHVD | Area (ha)= 5.75 Curve Number (CN)=76.50
| 02:200 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .262

Unit Hyd Qpeak (cms)= .838

PEAK FLOW      (cms)=    .051 (i)
TIME TO PEAK   (hrs)=     3.100
RUNOFF VOLUME  (mm)=    14.009
TOTAL RAINFALL (mm)=    44.800
RUNOFF COEFFICIENT =    .313

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0029-----
*
* Area 300
*
-----
| CALIB NASHVD | Area (ha)= 1.89 Curve Number (CN)=82.00
| 03:300 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .139

Unit Hyd Qpeak (cms)= .519

PEAK FLOW      (cms)=    .022 (i)
TIME TO PEAK   (hrs)=     3.000
RUNOFF VOLUME  (mm)=    17.240
TOTAL RAINFALL (mm)=    44.800
RUNOFF COEFFICIENT =    .385

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0030-----
*
* Area 400
*
-----
| CALIB NASHVD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.199

PEAK FLOW      (cms)=    .102 (i)
TIME TO PEAK   (hrs)=     5.067
RUNOFF VOLUME  (mm)=    11.516
TOTAL RAINFALL (mm)=    44.800
RUNOFF COEFFICIENT =    .257

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0031-----
*
* Area 500
*
-----
| CALIB NASHVD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .257

Unit Hyd Qpeak (cms)= .462

PEAK FLOW      (cms)=    .023 (i)
TIME TO PEAK   (hrs)=     5.033
RUNOFF VOLUME  (mm)=    11.516
TOTAL RAINFALL (mm)=    44.800
RUNOFF COEFFICIENT =    .257

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0032-----
*
*
*
*
*
*
*
*
*
*
* 5year - 12hr AES
*
-----
| READ STORM | Filename: C:\SWMMHYM-1\LAKEST-1\5AES12.stm
| Ptotal= 59.60 mm | Comments: 5 year AES 12hr

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 10.728 | 4.00 8.940 | 7.00 1.788 | 10.00 .000
2.00 12.516 | 5.00 8.344 | 8.00 .596 | 11.00 .000
3.00 11.920 | 6.00 4.768 | 9.00 .000 | 12.00 .000
```

```
-----
001:0033-----
*
*
*
* Area 100
*
-----
| CALIB NASHYD | Area (ha)= 1.46 Curve Number (CN)=76.50
| 01:100 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .192

Unit Hyd Qpeak (cms)= .290

PEAK FLOW (cms)= .022 (i)
TIME TO PEAK (hrs)= 3.033
RUNOFF VOLUME (mm)= 23.134
TOTAL RAINFALL (mm)= 59.600
RUNOFF COEFFICIENT = .388

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0034-----
*
*
* Area 200
*
-----
| CALIB NASHYD | Area (ha)= 5.75 Curve Number (CN)=76.50
| 02:200 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .262

Unit Hyd Qpeak (cms)= .838

PEAK FLOW (cms)= .085 (i)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 23.134
TOTAL RAINFALL (mm)= 59.600
RUNOFF COEFFICIENT = .388

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0035-----
*
*
* Area 300
*
-----
| CALIB NASHYD | Area (ha)= 1.89 Curve Number (CN)=82.00
| 03:300 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .139

Unit Hyd Qpeak (cms)= .519

PEAK FLOW (cms)= .035 (i)
TIME TO PEAK (hrs)= 3.000
RUNOFF VOLUME (mm)= 29.751
TOTAL RAINFALL (mm)= 59.600
RUNOFF COEFFICIENT = .466

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0036-----
*
*
* Area 400
*
-----
| CALIB NASHYD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.199

PEAK FLOW (cms)= .166 (i)
TIME TO PEAK (hrs)= 5.067
RUNOFF VOLUME (mm)= 19.400
TOTAL RAINFALL (mm)= 59.600
RUNOFF COEFFICIENT = .326

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0037-----
*
*
* Area 500
*
-----
| CALIB NASHYD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .257

Unit Hyd Qpeak (cms)= .462
```

```
PEAK FLOW (cms)= .038 (i)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 19.400
TOTAL RAINFALL (mm)= 59.600
RUNOFF COEFFICIENT = .326

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0038-----
*
*
*
*
*
* 10 year - 12hr AES
*
-----
| READ STORM | Filename: C:\SWHYM-1\LANEST-1\10AES12.stm
| Ptotal= 69.30 mm | Comments: 10 year AES 12hr
-----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 12.474 | 4.00 10.395 | 7.00 2.079 | 10.00 .000
2.00 14.553 | 5.00 9.702 | 8.00 .693 | 11.00 .000
3.00 13.860 | 6.00 5.544 | 9.00 .000 | 12.00 .000
-----
001:0039-----
*
*
*
* Area 100
*
-----
| CALIB NASHYD | Area (ha)= 1.46 Curve Number (CN)=76.50
| 01:100 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .192

Unit Hyd Qpeak (cms)= .290

PEAK FLOW (cms)= .029 (i)
TIME TO PEAK (hrs)= 3.033
RUNOFF VOLUME (mm)= 29.751
TOTAL RAINFALL (mm)= 69.300
RUNOFF COEFFICIENT = .429

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0040-----
*
*
* Area 200
*
-----
| CALIB NASHYD | Area (ha)= 5.75 Curve Number (CN)=76.50
| 02:200 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .262

Unit Hyd Qpeak (cms)= .838

PEAK FLOW (cms)= .110 (i)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 29.751
TOTAL RAINFALL (mm)= 69.300
RUNOFF COEFFICIENT = .429

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0041-----
*
*
* Area 300
*
-----
| CALIB NASHYD | Area (ha)= 1.89 Curve Number (CN)=82.00
| 03:300 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .139

Unit Hyd Qpeak (cms)= .519

PEAK FLOW (cms)= .045 (i)
TIME TO PEAK (hrs)= 3.000
RUNOFF VOLUME (mm)= 35.224
TOTAL RAINFALL (mm)= 69.300
RUNOFF COEFFICIENT = .508

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0042-----
*
*
* Area 400
*
-----
```

| CALIB NASHVD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.199

PEAK FLOW (cms)= .214 (1)
TIME TO PEAK (hrs)= 3.267
RUNOFF VOLUME (mm)= 25.224
TOTAL RAINFALL (mm)= 69.300
RUNOFF COEFFICIENT = .364

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0043-----
*
* Area 500
*

| CALIB NASHVD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .257

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .050 (1)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 25.224
TOTAL RAINFALL (mm)= 69.300
RUNOFF COEFFICIENT = .364

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0044-----
*
*
*
*
*
* 25 year - 12hr AES
*

| READ STORM | Filename: C:\SWMHYM-1\LAKEST-1\25AES12.stm
| Ptotal= 81.30 mm | Comments: 25 year AES 12hr

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 14.634 | 4.00 12.195 | 7.00 2.439 | 10.00 .000
2.00 17.073 | 5.00 11.382 | 8.00 .813 | 11.00 .000
3.00 16.260 | 6.00 6.504 | 9.00 .000 | 12.00 .000

001:0045-----
*
*
* Area 100
*

| CALIB NASHVD | Area (ha)= 1.46 Curve Number (CN)=76.50
| 01:100 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .192

Unit Hyd Qpeak (cms)= .290

PEAK FLOW (cms)= .037 (1)
TIME TO PEAK (hrs)= 3.033
RUNOFF VOLUME (mm)= 38.469
TOTAL RAINFALL (mm)= 81.300
RUNOFF COEFFICIENT = .473

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0046-----
*
* Area 200
*

| CALIB NASHVD | Area (ha)= 5.75 Curve Number (CN)=76.50
| 02:200 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .262

Unit Hyd Qpeak (cms)= .838

PEAK FLOW (cms)= .143 (1)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 38.469
TOTAL RAINFALL (mm)= 81.300
RUNOFF COEFFICIENT = .473

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0047-----
*
* Area 300
*

| CALIB NASHVD | Area (ha)= 1.89 Curve Number (CN)=82.00
| 03:300 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .139

Unit Hyd Qpeak (cms)= .519

PEAK FLOW (cms)= .057 (1)
TIME TO PEAK (hrs)= 3.000
RUNOFF VOLUME (mm)= 44.908
TOTAL RAINFALL (mm)= 81.300
RUNOFF COEFFICIENT = .552

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0048-----
*
* Area 400
*

| CALIB NASHVD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.199

PEAK FLOW (cms)= .282 (1)
TIME TO PEAK (hrs)= 3.233
RUNOFF VOLUME (mm)= 33.004
TOTAL RAINFALL (mm)= 81.300
RUNOFF COEFFICIENT = .406

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0049-----
*
* Area 500
*

| CALIB NASHVD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .257

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .066 (1)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 33.004
TOTAL RAINFALL (mm)= 81.300
RUNOFF COEFFICIENT = .406

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0050-----
*
*
*
*
* 50 year - 12hr AES
*

| READ STORM | Filename: C:\SWMHYM-1\LAKEST-1\50AES12.stm
| Ptotal= 90.40 mm | Comments: 50 year AES 12hr

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 16.272 | 4.00 13.560 | 7.00 2.712 | 10.00 .000
2.00 18.984 | 5.00 12.656 | 8.00 .904 | 11.00 .000
3.00 18.080 | 6.00 7.232 | 9.00 .000 | 12.00 .000

001:0051-----
*
*
* Area 100
*

| CALIB NASHVD | Area (ha)= 1.46 Curve Number (CN)=76.50
| 01:100 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

U.H. Tp(hrs)= .192

Unit Hyd Qpeak (cms)= .290

PEAK FLOW (cms)= .044 (1)
TIME TO PEAK (hrs)= 3.033
RUNOFF VOLUME (mm)= 45.400
TOTAL RAINFALL (mm)= 90.400
RUNOFF COEFFICIENT = .502

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0052-----

* Area 200

| CALIB NASHVD | Area (ha)= 5.75 Curve Number (CN)=76.50
| 02:200 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .262

Unit Hyd Qpeak (cms)= .838

PEAK FLOW (cms)= .169 (1)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 45.400
TOTAL RAINFALL (mm)= 90.400
RUNOFF COEFFICIENT = .502

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0053-----

* Area 300

| CALIB NASHVD | Area (ha)= 1.89 Curve Number (CN)=82.00
| 03:300 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .139

Unit Hyd Qpeak (cms)= .519

PEAK FLOW (cms)= .066 (1)
TIME TO PEAK (hrs)= 3.000
RUNOFF VOLUME (mm)= 52.512
TOTAL RAINFALL (mm)= 90.400
RUNOFF COEFFICIENT = .581

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0054-----

* Area 400

| CALIB NASHVD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.199

PEAK FLOW (cms)= .337 (1)
TIME TO PEAK (hrs)= 3.233
RUNOFF VOLUME (mm)= 39.259
TOTAL RAINFALL (mm)= 90.400
RUNOFF COEFFICIENT = .434

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0055-----

* Area 500

| CALIB NASHVD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .257

Unit Hyd Qpeak (cms)= .462

PEAK FLOW (cms)= .078 (1)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 39.259
TOTAL RAINFALL (mm)= 90.400
RUNOFF COEFFICIENT = .434

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0056-----

*

*
* 100 year - 12hr AES
*

| READ STORM | Filename: C:\SWMM\1\LAKEST-1\100AES12.stm
| Ptotal= 99.70 mm | Comments: 100 year AES 12hr

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
1.00	17.946	4.00	14.955	7.00	2.991	10.00	.000
2.00	20.937	5.00	13.958	8.00	.997	11.00	.000
3.00	19.940	6.00	7.976	9.00	.000	12.00	.000

001:0057-----

*
* Area 100
*

| CALIB NASHVD | Area (ha)= 1.46 Curve Number (CN)=76.50
| 01:100 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .192

Unit Hyd Qpeak (cms)= .290

PEAK FLOW (cms)= .051 (1)
TIME TO PEAK (hrs)= 3.033
RUNOFF VOLUME (mm)= 52.718
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT = .529

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0058-----

* Area 200

| CALIB NASHVD | Area (ha)= 5.75 Curve Number (CN)=76.50
| 02:200 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .262

Unit Hyd Qpeak (cms)= .838

PEAK FLOW (cms)= .196 (1)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 52.718
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT = .529

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0059-----

* Area 300

| CALIB NASHVD | Area (ha)= 1.89 Curve Number (CN)=82.00
| 03:300 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .139

Unit Hyd Qpeak (cms)= .519

PEAK FLOW (cms)= .076 (1)
TIME TO PEAK (hrs)= 3.000
RUNOFF VOLUME (mm)= 60.470
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT = .607

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0060-----

* Area 400

| CALIB NASHVD | Area (ha)= 14.13 Curve Number (CN)=71.00
| 04:400 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00

| U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.199

PEAK FLOW (cms)= .395 (1)
TIME TO PEAK (hrs)= 3.233
RUNOFF VOLUME (mm)= 45.920
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT = .461

(1) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0061-----
*
* Area 500
*

| CALIB NASHYD | Area (ha)= 3.11 Curve Number (CN)=71.00
| 05:500 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .257
*
Unit Hyd Qpeak (cms)= .462
PEAK FLOW (cms)= .092 (i)
TIME TO PEAK (hrs)= 3.067
RUNOFF VOLUME (mm)= 45.919
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT = .461

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0062-----
*

*
* PROPOSED CONDITION
*
*
* 25mm Quality Event
*

| READ STORM | Filename: C:\SWMHYD-1\LANEST-1\25MM.STM
| Ptotal= 25.00 mm | Comments: 25 mm 4 hr
*

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.17 2.071 | 1.17 5.696 | 2.17 5.194 | 3.17 2.799
.33 2.266 | 1.33 10.777 | 2.33 4.466 | 3.33 2.622
.50 2.524 | 1.50 50.214 | 2.50 3.949 | 3.50 2.476
.67 2.880 | 1.67 13.366 | 2.67 3.560 | 3.67 2.346
1.83 3.382 | 1.83 8.286 | 2.83 3.252 | 3.83 2.233
1.00 4.175 | 2.00 6.295 | 3.00 3.010 | 4.00 2.136

001:0063-----
*
* Area 101
*

| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
*

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .14 .14
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.90 2.90
Length (m)= 42.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 50.21 15.13
over (min)= 1.00 14.00
Storage Coeff. (min)= 1.45 (ii) 13.86 (ii)
Unit Hyd. Tpeak (min)= 1.00 14.00
Unit Hyd. peak (cms)= .85 .08
TOTALS
PEAK FLOW (cms)= .01 .00 .015 (iii)
TIME TO PEAK (hrs)= 1.50 1.70 1.500
RUNOFF VOLUME (mm)= 24.40 8.07 13.784
TOTAL RAINFALL (mm)= 25.00 25.00 24.996
RUNOFF COEFFICIENT = .98 .32 .551

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0064-----
*
* Area 201
*

| CALIB STANDHYD | Area (ha)= .33
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .17 .17
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.80 2.80
Length (m)= 20.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 50.21 15.74
over (min)= 1.00 13.00
Storage Coeff. (min)= .94 (ii) 13.28 (ii)
Unit Hyd. Tpeak (min)= 1.00 13.00
Unit Hyd. peak (cms)= 1.11 .09
TOTALS
PEAK FLOW (cms)= .02 .00 .018 (iii)
TIME TO PEAK (hrs)= 1.50 1.68 1.500
RUNOFF VOLUME (mm)= 24.40 8.07 13.784
TOTAL RAINFALL (mm)= 25.00 25.00 24.996
RUNOFF COEFFICIENT = .98 .32 .551

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0065-----
*
* Area 301
*

| CALIB STANDHYD | Area (ha)= 8.44
| 03:301 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 25.00
*

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 5.06 3.38
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 700.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 50.21 22.69
over (min)= 7.00 15.00
Storage Coeff. (min)= 6.71 (ii) 15.03 (ii)
Unit Hyd. Tpeak (min)= 7.00 15.00
Unit Hyd. peak (cms)= .17 .08
TOTALS
PEAK FLOW (cms)= .22 .13 .299 (iii)
TIME TO PEAK (hrs)= 1.55 1.72 1.583
RUNOFF VOLUME (mm)= 24.40 8.58 12.532
TOTAL RAINFALL (mm)= 25.00 25.00 24.996
RUNOFF COEFFICIENT = .98 .34 .501

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0066-----
*
* Total Flows to Pond
*
* 24 hour draw down of 25 mm runoff
*
* 1058 m3 / 24 hr / 60 min per hr / 60 s per min = 0.012 cms
*

| COMPUTE VOLUME |
| ID:03 (301) | DISCHARGE TIME

(cms) (hrs)
START CONTROLLING AT .000 .267
INFLOW HYD. PEAKS AT .299 1.583
STOP CONTROLLING AT .012 4.331
REQUIRED STORAGE VOLUME (ha.m.)= .0960
TOTAL HYDROGRAPH VOLUME (ha.m.)= .1058
% OF HYDROGRAPH TO STORE = 90.7307

NOTE: Storage was computed to reduce the Inflow
peak to .012 (cms).

*** WARNING: Calculated volume may not be the maximum.

001:0067-----
*
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| INP:03:(301) |
OUT:04:(POND)
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .059 .3300E+00

```

.007 .3000E+01 | .062 .3600E+00
.009 .6000E+01 | .065 .3900E+00
.011 .9000E+01 | .068 .4200E+00
.026 .1200E+00 | .070 .4500E+00
.033 .1500E+00 | .073 .4800E+00
.039 .1800E+00 | .075 .5100E+00
.043 .2100E+00 | .077 .5400E+00
.048 .2400E+00 | .529 .5700E+00
.052 .2700E+00 | .000 .0000E+00
.055 .3000E+00 | .000 .0000E+00

ROUTING RESULTS      AREA   QPEAK   TPEAK   R.V.
-----
INFLW >03: (301 )   8.44   .299   1.583  12.532
OUTFLOW>04: (POND ) 8.44   .013   4.300  12.532
OVERFLOW***: (000001) .00   .000   .000   .000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.452
TIME SHIFT OF PEAK FLOW (min)= 163.00
MAXIMUM STORAGE USED (ha.m.)=-.9388E-01

-----
001:0068-----
*
* Area 401
*
-----
| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
|-----
| U.N. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.136

PEAK FLOW (cms)= .072 (i)
TIME TO PEAK (hrs)= 2.133
RUNOFF VOLUME (mm)= 3.711
TOTAL RAINFALL (mm)= 24.996
RUNOFF COEFFICIENT = .148

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0069-----
*
* Area 501
*
-----
| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(h)= 65.00 Dir. Conn.(%)= 35.00
|-----
| IMPERVIOUS PERVIOUS (i)
| Surface Area (ha)= 2.55 1.37
| Dep. Storage (mm)= .60 2.50
| Average Slope (%)= 4.90 6.40
| Length (m)= 500.00 35.00
| Mannings n = .013 .250

Max.eff.Inten.(mm/hr)= 50.21 23.12
over (min) 5.00 14.00
Storage Coeff. (min)= 5.49 (ii) 13.74 (ii)
Unit Hyd. Tpeak (min)= 5.00 14.00
Unit Hyd. peak (cms)= .21 .08

*TOTALS*
PEAK FLOW (cms)= .16 .06
TIME TO PEAK (hrs)= 1.52 1.70
RUNOFF VOLUME (mm)= 24.40 8.52 14.075
TOTAL RAINFALL (mm)= 25.00 25.00 24.996
RUNOFF COEFFICIENT = .98 .34 .563

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0070-----
*
* Total Flows to Pond
*
* 24 hour draw down of 25 mm runoff
*
* 552 m3 / 24 hr / 60 min per hr / 60 a per min = 0.006 cms
*
-----
| COMPUTE VOLUME |
| ID:06 (501 ) |
|-----
| DISCHARGE TIME
| (cms) (hrs)
| START CONTROLLING AT .000 .267
| INFLW HYD. PEAKS AT .185 1.533
| STOP CONTROLLING AT .012 4.122
```

```

REQUIRED STORAGE VOLUME (ha.m.)= .0462
TOTAL HYDROGRAPH VOLUME (ha.m.)= .0552
% OF HYDROGRAPH TO STORE = 83.6759

NOTE: Storage was computed to reduce the Inflow
peak to .012 (cms).

*** WARNING: Calculated volume may not be the maximum.
```

```

-----
001:0071-----
*
-----
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| ID:06 (501 ) |
| OUT<07: (POND ) |
|-----
| OUTFLOW STORAGE TABLE -----
| OUTFLOW STORAGE | OUTFLOW STORAGE
| (cms) (ha.m.) | (cms) (ha.m.)
| .000 .0000E+00 | .074 .1200E+00
| .004 .1500E-01 | .080 .1350E+00
| .005 .3000E-01 | .086 .1500E+00
| .006 .4500E-01 | .092 .1650E+00
| .036 .6000E-01 | .098 .1800E+00
| .048 .7500E-01 | .325 .1950E+00
| .058 .9000E-01 | .735 .2100E+00
| .066 .1050E+00 | .000 .0000E+00

ROUTING RESULTS      AREA   QPEAK   TPEAK   R.V.
-----
INFLW >06: (501 )   3.92   .185   1.533  14.075
OUTFLOW<07: (POND ) 3.92   .012   4.117  14.074
OVERFLOW***: (000001) .00   .000   .000   .000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin](%)= 6.251
TIME SHIFT OF PEAK FLOW (min)= 155.00
MAXIMUM STORAGE USED (ha.m.)=-.4764E-01

-----
001:0072-----
*
*****
*****
*****
*
*
* 100 year event - 1 hr Chicago
*
-----
| CHICAGO STORM | IDF curve parameters: A= 971.139
| Ptotal= 48.61 mm | B= 1.500
|-----
| C= .726
| used in: INTENSITY = A / (t + B)^C

Duration of storm = 1.00 hrs
Storm time step = 2.00 min
Time to peak ratio = .33

The CORRELATION coefficient is = .9996862

TIME ENTERED COMPUTED
(min) (mm/hr) (mm/hr)
5. 268.10 249.52
10. 165.10 164.90
15. 124.40 126.88
30. 76.60 79.34
60. 47.20 48.82
120. 29.10 29.78
360. 13.50 13.49
720. 8.30 8.17
1440. 5.10 4.94

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.03 15.562 | .30 121.721 | .57 32.195 | .83 17.704
.07 17.083 | .33 391.100 | .60 28.944 | .87 16.846
.10 19.009 | .37 155.358 | .63 26.366 | .90 16.081
.13 21.539 | .40 89.546 | .67 24.267 | .93 15.393
.17 25.035 | .43 64.172 | .70 22.521 | .97 14.770
.20 30.231 | .47 50.663 | .73 21.043 | 1.00 14.204
.23 38.904 | .50 42.230 | .77 19.774 |
.27 56.826 | .53 36.437 | .80 18.672 |
```

```

-----
001:0073-----
*
* Area 101
*
-----
```

| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.14	
Dep. Storage (mm)=	.60	2.50
Average Slope (%)=	2.90	2.90
Length (m)=	42.00	35.00
Mannings n	.013	.250
Max.eff.Inten.(mm/hr)=	391.10	144.56
over (min)	1.00	6.00
Storage Coeff. (min)=	.64 (ii)	5.67 (ii)
Unit Hyd. Tpeak (min)=	1.00	6.00
Unit Hyd. peak (cms)=	1.34	.20
PEAK FLOW (cms)=	.10	.03
TIME TO PEAK (hrs)=	.33	.43
RUNOFF VOLUME (mm)=	48.21	24.48
TOTAL RAINFALL (mm)=	48.81	48.81
RUNOFF COEFFICIENT	.99	.50

TOTALS

PEAK FLOW (cms)= .112 (iii)

TIME TO PEAK (hrs)= .333

RUNOFF VOLUME (mm)= 32.787

TOTAL RAINFALL (mm)= 48.806

RUNOFF COEFFICIENT = .672

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0074-----

* Area 201
*

| CALIB STANDHYD | Area (ha)= .32
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.16	
Dep. Storage (mm)=	.60	2.50
Average Slope (%)=	2.80	2.80
Length (m)=	20.00	35.00
Mannings n	.013	.250
Max.eff.Inten.(mm/hr)=	391.10	158.24
over (min)	1.00	5.00
Storage Coeff. (min)=	.41 (ii)	5.32 (ii)
Unit Hyd. Tpeak (min)=	1.00	5.00
Unit Hyd. peak (cms)=	1.55	.22
PEAK FLOW (cms)=	.12	.04
TIME TO PEAK (hrs)=	.33	.42
RUNOFF VOLUME (mm)=	48.21	24.48
TOTAL RAINFALL (mm)=	48.81	48.81
RUNOFF COEFFICIENT	.99	.50

TOTALS

PEAK FLOW (cms)= .134 (iii)

TIME TO PEAK (hrs)= .333

RUNOFF VOLUME (mm)= 32.787

TOTAL RAINFALL (mm)= 48.806

RUNOFF COEFFICIENT = .672

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0075-----

* Area 301
*

| CALIB STANDHYD | Area (ha)= 8.44
| 03:301 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 25.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	5.06	3.38
Dep. Storage (mm)=	.60	2.50
Average Slope (%)=	4.90	6.40
Length (m)=	700.00	35.00
Mannings n	.013	.250
Max.eff.Inten.(mm/hr)=	312.52	196.42
over (min)	3.00	7.00
Storage Coeff. (min)=	3.23 (ii)	6.74 (ii)
Unit Hyd. Tpeak (min)=	3.00	7.00
Unit Hyd. peak (cms)=	.36	.17
PEAK FLOW (cms)=	1.22	1.13
TIME TO PEAK (hrs)=	.37	.45
RUNOFF VOLUME (mm)=	48.21	25.30
TOTAL RAINFALL (mm)=	48.81	48.81
RUNOFF COEFFICIENT	.99	.52

TOTALS

PEAK FLOW (cms)= 1.895 (iii)

TIME TO PEAK (hrs)= .417

RUNOFF VOLUME (mm)= 31.025

TOTAL RAINFALL (mm)= 48.806

RUNOFF COEFFICIENT = .636

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0076-----

| COMPUTE VOLUME | DISCHARGE TIME
| ID:03 (301) | (cms) (hrs)
START CONTROLLING AT .000 .033
INFLOW HYD. PEAKS AT 1.895 .417
STOP CONTROLLING AT .220 1.077
REQUIRED STORAGE VOLUME (ha.m.)= .2119
TOTAL HYDROGRAPH VOLUME (ha.m.)= .2619
% OF HYDROGRAPH TO STORE = 80.9357

NOTE: Storage was computed to reduce the Inflow
peak to .220 (cms).

*** WARNING: Calculated volume may not be the maximum.

001:0077-----

* Area 401
*

| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.136

PEAK FLOW (cms)= .509 (i)
TIME TO PEAK (hrs)= .967
RUNOFF VOLUME (mm)= 14.078
TOTAL RAINFALL (mm)= 48.806
RUNOFF COEFFICIENT = .288

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0078-----

* Area 501
*

| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 35.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	2.55	1.37
Dep. Storage (mm)=	.60	2.50
Average Slope (%)=	4.90	6.40
Length (m)=	500.00	35.00
Mannings n	.013	.250
Max.eff.Inten.(mm/hr)=	312.52	212.32
over (min)	3.00	6.00
Storage Coeff. (min)=	2.64 (ii)	6.04 (ii)
Unit Hyd. Tpeak (min)=	3.00	6.00
Unit Hyd. peak (cms)=	.41	.19
PEAK FLOW (cms)=	.86	.48
TIME TO PEAK (hrs)=	.37	.43
RUNOFF VOLUME (mm)=	48.21	25.17
TOTAL RAINFALL (mm)=	48.81	48.81
RUNOFF COEFFICIENT	.99	.52

TOTALS

PEAK FLOW (cms)= 1.141 (iii)

TIME TO PEAK (hrs)= .367

RUNOFF VOLUME (mm)= 33.236

TOTAL RAINFALL (mm)= 48.806

RUNOFF COEFFICIENT = .681

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0079-----

| COMPUTE VOLUME | DISCHARGE TIME
| ID:06 (501) | (cms) (hrs)
START CONTROLLING AT .000 .033
INFLOW HYD. PEAKS AT 1.141 .367
STOP CONTROLLING AT .162 .963
REQUIRED STORAGE VOLUME (ha.m.)= .0949
TOTAL HYDROGRAPH VOLUME (ha.m.)= .1303
% OF HYDROGRAPH TO STORE = 72.8772

NOTE: Storage was computed to reduce the Inflow
peak to .162 (cms).

*** WARNING: Calculated volume may not be the maximum.

001:0080-----
*

*
* 100 year event - 4 hr Chicago

CHICAGO STORM | IDF curve parameters: A= 971.139
Ptotal= 72.33 mm | B= 1.500
C= -.726
used in: INTENSITY = A / (t + B)^C
Duration of storm = 4.00 hrs
Storm time step = 2.00 min
Time to peak ratio = .33

The CORRELATION coefficient is = .9996862

TIME (min)	ENTERED (mm/hr)	COMPUTED (mm/hr)
5.	268.10	249.52
10.	165.10	164.90
15.	124.40	126.88
30.	76.60	79.34
60.	47.20	48.82
120.	29.10	29.78
360.	13.50	13.49
720.	8.10	8.17
1440.	5.10	4.94

TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr	TIME hrs	RAIN mm/hr
.03	5.110	1.03	15.562	2.03	13.687	3.03	7.038
.07	5.209	1.07	17.083	2.07	13.212	3.07	6.937
.10	5.314	1.10	19.009	2.10	12.774	3.10	6.840
.13	5.423	1.13	21.539	2.13	12.369	3.13	6.746
.17	5.537	1.17	25.035	2.17	11.993	3.17	6.655
.20	5.658	1.20	30.231	2.20	11.644	3.20	6.567
.23	5.785	1.23	38.904	2.23	11.317	3.23	6.481
.27	5.919	1.27	56.826	2.27	11.011	3.27	6.399
.30	6.060	1.30	121.721	2.30	10.725	3.30	6.318
.33	6.210	1.33	391.100	2.33	10.455	3.33	6.240
.37	6.369	1.37	155.358	2.37	10.201	3.37	6.164
.40	6.538	1.40	89.546	2.40	9.961	3.40	6.091
.43	6.719	1.43	64.172	2.43	9.734	3.43	6.019
.47	6.911	1.47	50.663	2.47	9.519	3.47	5.950
.50	7.117	1.50	42.230	2.50	9.314	3.50	5.882
.53	7.338	1.53	36.437	2.53	9.120	3.53	5.816
.57	7.576	1.57	32.195	2.57	8.936	3.57	5.752
.60	7.834	1.60	28.944	2.60	8.760	3.60	5.689
.63	8.113	1.63	26.366	2.63	8.591	3.63	5.628
.67	8.417	1.67	24.267	2.67	8.431	3.67	5.569
.70	8.750	1.70	22.521	2.70	8.277	3.70	5.511
.73	9.116	1.73	21.043	2.73	8.130	3.73	5.454
.77	9.520	1.77	19.774	2.77	7.989	3.77	5.399
.80	9.969	1.80	18.672	2.80	7.853	3.80	5.345
.83	10.473	1.83	17.704	2.83	7.723	3.83	5.293
.87	11.041	1.87	16.846	2.87	7.598	3.87	5.241
.90	11.688	1.90	16.081	2.90	7.478	3.90	5.191
.93	12.432	1.93	15.393	2.93	7.362	3.93	5.142
.97	13.300	1.97	14.770	2.97	7.250	3.97	5.094
1.00	14.326	2.00	14.204	3.00	7.142	4.00	5.047

001:0081-----
*
* Area 101

CALIB STANDHYD | Area (ha)= .28
01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.14	.14
Dep. Storage (mm)=	.60	2.50
Average Slope (%)=	2.90	2.90
Length (m)=	42.00	35.00
Mannings n =	.013	.250
Max.eff.Inten.(mm/hr)=	391.10	190.86
over (min)=	1.00	5.00
Storage Coeff. (min)=	.64 (ii)	5.14 (ii)
Unit Hyd. Tpeak (min)=	1.00	5.00
Unit Hyd. peak (cms)=	1.34	.22
PEAK FLOW (cms)=	.10	.05
TIME TO PEAK (hrs)=	1.33	1.40
RUNOFF VOLUME (mm)=	71.73	43.76

TOTAL RAINFALL (mm)= 72.33 72.33 72.334
RUNOFF COEFFICIENT = .99 .60 .740

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0082-----
*
* Area 201

CALIB STANDHYD | Area (ha)= .32
02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	.16	.16
Dep. Storage (mm)=	.60	2.50
Average Slope (%)=	2.80	2.80
Length (m)=	20.00	35.00
Mannings n =	.013	.250
Max.eff.Inten.(mm/hr)=	391.10	190.86
over (min)=	1.00	5.00
Storage Coeff. (min)=	.41 (ii)	4.96 (ii)
Unit Hyd. Tpeak (min)=	1.00	5.00
Unit Hyd. peak (cms)=	1.55	.23
PEAK FLOW (cms)=	.12	.05
TIME TO PEAK (hrs)=	1.33	1.40
RUNOFF VOLUME (mm)=	71.73	43.76
TOTAL RAINFALL (mm)=	72.33	72.334
RUNOFF COEFFICIENT =	.99	.60

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0083-----
*
* Area 301

CALIB STANDHYD | Area (ha)= 8.44
03:301 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 25.00

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha)=	5.06	3.38
Dep. Storage (mm)=	.60	2.50
Average Slope (%)=	4.90	6.40
Length (m)=	700.00	35.00
Mannings n =	.013	.250
Max.eff.Inten.(mm/hr)=	312.52	255.40
over (min)=	3.00	6.00
Storage Coeff. (min)=	3.23 (ii)	6.39 (ii)
Unit Hyd. Tpeak (min)=	3.00	6.00
Unit Hyd. peak (cms)=	.36	.18
PEAK FLOW (cms)=	1.23	1.48
TIME TO PEAK (hrs)=	1.37	1.42
RUNOFF VOLUME (mm)=	71.73	44.76
TOTAL RAINFALL (mm)=	72.33	72.334
RUNOFF COEFFICIENT =	.99	.62

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0084-----
*
*

COMPUTE VOLUME	DISCHARGE	TIME
ID:03 (301)	(cms)	(hrs)
START CONTROLLING AT	.000	.100
INFLW HYD. PEAKS AT	2.379	1.400
STOP CONTROLLING AT	.289	2.132
REQUIRED STORAGE VOLUME (ha.m.)=		.2173
TOTAL HYDROGRAPH VOLUME (ha.m.)=		.4347
% OF HYDROGRAPH TO STORE =		49.9784

NOTE: Storage was computed to reduce the Inflow
peak to .289 (cms).

2.00 7.686 | 4.00 10.113 | 6.00 3.236 |

```
001:0089-----
*
*
* Area 101
*
-----
| CALIB STANDHYD |      Area      (ha)=    .28
| 01:101   DT= 1.00 | Total Imp(k)=    50.00 Dir. Conn.(%)=    35.00
```

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha) =	.14	.14
Dep. Storage (mm) =	.60	2.50
Average Slope (%) =	2.90	2.90
Length (m) =	42.00	35.00
Mannings n =	.013	.250

Max.eff.Inten. (mm/hr)-	50.56	53.79
over (min)	1.00	9.00
Storage Coeff. (min)-	1.45 (ii)	8.92 (ii)
Unit Hyd. Tpeak (min)-	1.00	9.00
Unit Hyd. peak (cms)-	.85	.13

			TOTALS
PEAK FLOW	(cms)-	.01	.034 (iii)
TIME TO PEAK	(hrs)-	2.78	3.00
RUNOFF VOLUME	(mm)-	80.30	51.18
TOTAL RAINFALL	(mm)-	80.90	80.90
RUNOFF COEFFICIENT	=	.99	.759

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY

-----0090-----
Area 201

```

-----
| CALIB STANDHYD | Area (ha)= .32
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

```

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha) =	.16	.16
Dep. Storage (mm) =	.60	2.50
Average Slope (%) =	2.80	2.80
Length (m) =	20.00	35.00
Mannings n =	.013	.250

Max.eff.Inten.(mm/hr)=	50.56	53.89
over (min)	1.00	8.00
Storage Coeff. (min)=	.94 (ii)	8.48 (ii)
Unit Hyd. Tpeak (min)=	1.00	8.00
Unit Hyd. peak (cms)=	1.11	.14

	1962	1963	1964
PEAK FLOW (cms) =	.02	.02	.039 (iii)
TIME TO PEAK (hrs) =	2.78	3.00	3.000
RUNOFF VOLUME (mm) =	80.30	51.18	61.373
TOTAL RAINFALL (mm) =	80.90	80.90	80.900
RUNOFF COEFFICIENT =	.99	.63	.759

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY

```
001:0091-----
*
* Area 301
```

-----		Area (ha)=	8.44		
CALIB STANDHYD	03:301 DT= 1.00	Total Imp(%)=	60.00	Dir. Conn.(%)=	25.00

		IMPERVIOUS	PERVIOUS (i)
Surface Area	(ha) =	5.06	3.38
Dep. Storage	(mm) =	.60	2.50
Average Slope	(%) =	4.90	6.40
Length	(m) =	700.00	35.00
Mannings n	=	.013	.250

Max. eff. Inten. (mm/hr) =	50.56	77.92
over (min)	7.00	12.00
Storage Coeff. (min) =	6.70 (ii)	11.77 (ii)
Unit Hyd. Tpeak (min) =	7.00	12.00
Unit Hyd. peak (cms) =	.17	.10

PEAK FLOW	(cms) =	.30	.68	.977 (iii)
-----------	---------	-----	-----	------------

TIME TO PEAK (hrs)= 3.00 3.02 3.000
RUNOFF VOLUME (mm)= 80.30 52.24 59.257
TOTAL RAINFALL (mm)= 80.90 80.90 80.900
RUNOFF COEFFICIENT = .99 .65 .732

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0092-----
*

| COMPUTE VOLUME |
| ID:03 (301) | | DISCHARGE TIME
|-----| (cms) (hrs)
START CONTROLLING AT .000 .100
INFLW HYD. PEAKS AT .977 3.000
STOP CONTROLLING AT .191 4.114
REQUIRED STORAGE VOLUME (ha.m.)= .2946
TOTAL HYDROGRAPH VOLUME (ha.m.)= .5001
% OF HYDROGRAPHE TO STORE = 58.9072
NOTE: Storage was computed to reduce the Inflow
peak to .191 (cms).
*** WARNING: Calculated volume may not be the maximum.

001:0093-----
*
* Area 401
*

| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia 4.000 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .450
Unit Hyd Qpeak (cms)= 1.136
PEAK FLOW (cms)= .761 (i)
TIME TO PEAK (hrs)= 3.200
RUNOFF VOLUME (mm)= 33.850
TOTAL RAINFALL (mm)= 80.900
RUNOFF COEFFICIENT = .418
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0094-----
*
* Area 501
*

| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 35.00
|-----|
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 2.55 1.37
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 500.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 50.56 77.14
over (min)= 5.00 11.00
Storage Coeff. (min)= 5.47 (ii) 10.57 (ii)
Unit Hyd. Tpeak (min)= 5.00 11.00
Unit Hyd. peak (cms)= .21 .11
TOTALS
PEAK FLOW (cms)= .19 .28 .470 (iii)
TIME TO PEAK (hrs)= 3.00 3.02 3.000
RUNOFF VOLUME (mm)= 80.30 52.06 61.944
TOTAL RAINFALL (mm)= 80.90 80.90 80.900
RUNOFF COEFFICIENT = .99 .64 .766

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0095-----
*

| COMPUTE VOLUME |
| ID:06 (501) | | DISCHARGE TIME
|-----| (cms) (hrs)
START CONTROLLING AT .000 .100
INFLW HYD. PEAKS AT .470 3.000
STOP CONTROLLING AT .212 3.249

REQUIRED STORAGE VOLUME (ha.m.)= .0806
TOTAL HYDROGRAPH VOLUME (ha.m.)= .2428
% OF HYDROGRAPH TO STORE = 33.2100

NOTE: Storage was computed to reduce the Inflow
peak to .212 (cms).

*** WARNING: Calculated volume may not be the maximum.

001:0096-----
*

| HEAD STORM | Filename: C:\SNMHYM-1\LAWEST-1\100SCS12
| Ptotal= 99.70 mm | Comments: 100year SCS 12hr
|-----|
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 2.493 | 4.00 4.486 | 7.00 9.970 | 10.00 3.490
2.00 2.493 | 5.00 8.474 | 8.00 2.243 | 11.00 3.490
3.00 3.988 | 6.00 52.343 | 9.00 2.243 | 12.00 3.988

001:0097-----
*
* Area 101
*

| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
|-----|
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .14 .14
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.90 2.90
Length (m)= 42.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 52.34 57.93
over (min)= 1.00 9.00
Storage Coeff. (min)= 1.43 (ii) 8.68 (ii)
Unit Hyd. Tpeak (min)= 1.00 9.00
Unit Hyd. peak (cms)= .86 .13
TOTALS
PEAK FLOW (cms)= .01 .02 .036 (iii)
TIME TO PEAK (hrs)= 5.65 6.00 6.000
RUNOFF VOLUME (mm)= 99.10 67.96 78.862
TOTAL RAINFALL (mm)= 99.70 99.70 99.701
RUNOFF COEFFICIENT = .99 .68 .791

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0098-----
*
* Area 201
*

| CALIB STANDHYD | Area (ha)= .32
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
|-----|
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .16 .16
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.80 2.80
Length (m)= 20.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 52.34 58.01
over (min)= 1.00 8.00
Storage Coeff. (min)= .93 (ii) 8.25 (ii)
Unit Hyd. Tpeak (min)= 1.00 8.00
Unit Hyd. peak (cms)= 1.12 .14
TOTALS
PEAK FLOW (cms)= .02 .03 .041 (iii)
TIME TO PEAK (hrs)= 5.62 6.00 6.000
RUNOFF VOLUME (mm)= 99.10 67.96 78.862
TOTAL RAINFALL (mm)= 99.70 99.70 99.701
RUNOFF COEFFICIENT = .99 .68 .791

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0099-----
*
* Area 301
*

| CALIB STANDHYD | Area (ha)= 8.44
| 03:301 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 25.00

IMPERVIOUS PVIOUS (i)
Surface Area (ha)= 5.06 3.38
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 700.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 52.34 83.89
over (min) 7.00 12.00
Storage Coeff. (min)= 6.60 (ii) 11.53 (ii)
Unit Hyd. Tpeak (min)= 7.00 12.00
Unit Hyd. peak (cms)= .17 .10
TOTALS
PEAK FLOW (cms)= .31 .75 1.054 (iii)
TIME TO PEAK (hrs)= 6.00 6.02 6.000
RUNOFF VOLUME (mm)= 99.09 69.11 76.618
TOTAL RAINFALL (mm)= 99.70 99.70 99.701
RUNOFF COEFFICIENT = .99 .69 .768
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0100-----
*
*

| COMPUTE VOLUME |
| ID:03 (301) | DISCHARGE TIME

(cms) (hrs)
START CONTROLLING AT .000 .233
INFLOW HYD. PEAKS AT 1.054 6.000
STOP CONTROLLING AT .211 7.049
REQUIRED STORAGE VOLUME (ha.m.)= .3007
TOTAL HYDROGRAPH VOLUME (ha.m.)= .6467
% OF HYDROGRAPH TO STORE = 46.5036
NOTE: Storage was computed to reduce the Inflow
peak to .211 (cms).
*** WARNING: Calculated volume may not be the maximum.

001:0101-----
*
* Area 401
*

| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia (mm)= 4.000 % of Linear Res.(N)= 3.00

U.N. Tp (hrs)= .450
Unit Hyd Qpeak (cms)= 1.136
PEAK FLOW (cms)= .908 (i)
TIME TO PEAK (hrs)= 6.167
RUNOFF VOLUME (mm)= 47.331
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT = .475
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0102-----
*
* Area 501
*

| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 35.00

IMPERVIOUS PVIOUS (i)
Surface Area (ha)= 2.55 1.37
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 500.00 35.00
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 52.34 83.15
over (min) 5.00 10.00
Storage Coeff. (min)= 5.40 (ii) 10.34 (ii)
Unit Hyd. Tpeak (min)= 5.00 10.00
Unit Hyd. peak (cms)= .21 .11
TOTALS
PEAK FLOW (cms)= .20 .30 .504 (iii)
TIME TO PEAK (hrs)= 6.00 6.00 6.000
RUNOFF VOLUME (mm)= 99.09 68.91 79.481
TOTAL RAINFALL (mm)= 99.70 99.70 99.701
RUNOFF COEFFICIENT = .99 .69 .797
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0103-----
*

| COMPUTE VOLUME | DISCHARGE TIME
| ID:06 (501) | (cms) (hrs)

START CONTROLLING AT .000 .233
INFLOW HYD. PEAKS AT .504 6.000
STOP CONTROLLING AT .248 6.210
REQUIRED STORAGE VOLUME (ha.m.)= .0750
TOTAL HYDROGRAPH VOLUME (ha.m.)= .3116
% OF HYDROGRAPH TO STORE = 24.0687
NOTE: Storage was computed to reduce the Inflow
peak to .248 (cms).
*** WARNING: Calculated volume may not be the maximum.

001:0104-----
*
*

| READ STORM | Filename: C:\SWHMYM-1\LAKEST-1\2AES12.stm
| Total= 44.80 mm | Comments: 2 year AES 12hr

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 8.964 | 4.00 6.720 | 7.00 1.344 | 10.00 .000
2.00 9.408 | 5.00 6.272 | 8.00 .448 | 11.00 .000
3.00 8.960 | 6.00 3.584 | 9.00 .000 | 12.00 .000

001:0105-----
*
* Area 101
*

| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

IMPERVIOUS PVIOUS (i)
Surface Area (ha)= .14 .14
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.90 2.90
Length (m)= 42.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 9.41 6.71
over (min) 3.00 20.00
Storage Coeff. (min)= 2.84 (ii) 20.01 (ii)
Unit Hyd. Tpeak (min)= 3.00 20.00
Unit Hyd. peak (cms)= .39 .06
TOTALS
PEAK FLOW (cms)= .00 .00 .005 (iii)
TIME TO PEAK (hrs)= 1.82 3.13 3.000
RUNOFF VOLUME (mm)= 44.20 21.43 29.403
TOTAL RAINFALL (mm)= 44.80 44.80 44.800
RUNOFF COEFFICIENT = .99 .48 .656
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
001:0106-----
*
* Area 201
*
| CALIB STANDHYD | Area (ha)= .32
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .16 .16
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.80 2.80
Length (m)= 20.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 9.41 6.72
over (min) 2.00 19.00
Storage Coeff. (min)= 1.84 (ii) 19.18 (ii)
Unit Hyd. Tpeak (min)= 2.00 19.00
Unit Hyd. peak (cms)= .59 .06
*TOTALS*
PEAK FLOW (cms)= .00 .00 .006 (iii)
TIME TO PEAK (hrs)= 1.75 3.12 3.000
RUNOFF VOLUME (mm)= 44.20 21.43 29.403
TOTAL RAINFALL (mm)= 44.80 44.80 44.800
RUNOFF COEFFICIENT = .99 .48 .656
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
```

```
-----
001:0107-----
*
* Area 301
*
| CALIB STANDHYD | Area (ha)= 8.44
| 03:301 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 25.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 5.06 3.38
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 700.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 9.41 9.88
over (min) 13.00 25.00
Storage Coeff. (min)= 13.12 (ii) 24.72 (ii)
Unit Hyd. Tpeak (min)= 13.00 25.00
Unit Hyd. peak (cms)= .09 .05
*TOTALS*
PEAK FLOW (cms)= .05 .09 .137 (iii)
TIME TO PEAK (hrs)= 2.02 3.20 3.067
RUNOFF VOLUME (mm)= 44.20 22.20 27.705
TOTAL RAINFALL (mm)= 44.80 44.80 44.800
RUNOFF COEFFICIENT = .99 .50 .618
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
```

```
-----
001:0108-----
*
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>03:(301 ) |
| OUT<04:(POND ) |
-----
***** OUTFLOW STORAGE TABLE *****
OUTFLOW STORAGE OUTFLOW STORAGE
(cms) (ha.m.) (cms) (ha.m.)
.000 .0000E+00 | .059 .3300E+00
.007 .3000E-01 | .062 .3600E+00
.009 .6000E-01 | .065 .3900E+00
.011 .9000E-01 | .068 .4200E+00
.026 .1200E+00 | .070 .4500E+00
.033 .1500E+00 | .073 .4800E+00
.039 .1800E+00 | .075 .5100E+00
.043 .2100E+00 | .077 .5400E+00
.048 .2400E+00 | .529 .5700E+00
.052 .2700E+00 | .000 .0000E+00
.055 .3000E+00 | .000 .0000E+00
ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >03: (301 ) 8.44 .137 3.067 27.705
OUTFLOW<04: (POND ) 8.44 .038 6.667 27.704
OVERFLOW***: (000001) .00 .000 .000 .000
-----
```

```
TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00
```

```
PEAK FLOW REDUCTION (Qout/Qin)(%)= 27.702
TIME SHIFT OF PEAK FLOW (min)= 216.00
MAXIMUM STORAGE USED (ha.m.)=.1762E+00
```

```
-----
001:0109-----
*
* Area 401
*
| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
| | U.H. Tp(hrs)= .450
Unit Hyd Qpeak (cms)= 1.136
PEAK FLOW (cms)= .101 (i)
TIME TO PEAK (hrs)= 5.067
RUNOFF VOLUME (mm)= 12.010
TOTAL RAINFALL (mm)= 44.800
RUNOFF COEFFICIENT = .268
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
```

```
-----
001:0110-----
*
* Area 501
*
| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 35.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 2.55 1.37
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 500.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 9.41 9.78
over (min) 11.00 22.00
Storage Coeff. (min)= 10.72 (ii) 22.37 (ii)
Unit Hyd. Tpeak (min)= 11.00 22.00
Unit Hyd. peak (cms)= .10 .05
*TOTALS*
PEAK FLOW (cms)= .04 .03 .068 (iii)
TIME TO PEAK (hrs)= 2.00 3.15 3.033
RUNOFF VOLUME (mm)= 44.20 22.09 29.830
TOTAL RAINFALL (mm)= 44.80 44.80 44.800
RUNOFF COEFFICIENT = .99 .49 .666
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
```

```
-----
001:0111-----
*
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>06:(501 ) |
| OUT<07:(POND ) |
-----
***** OUTFLOW STORAGE TABLE *****
OUTFLOW STORAGE OUTFLOW STORAGE
(cms) (ha.m.) (cms) (ha.m.)
.000 .0000E+00 | .074 .1200E+00
.004 .1500E-01 | .080 .1350E+00
.005 .3000E-01 | .086 .1500E+00
.006 .4500E-01 | .092 .1650E+00
.036 .6000E-01 | .098 .1800E+00
.048 .7500E-01 | .325 .1950E+00
.058 .9000E-01 | .735 .2100E+00
.066 .1050E+00 | .000 .0000E+00
ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >06: (501 ) 3.92 .068 3.033 29.830
OUTFLOW<07: (POND ) 3.92 .041 5.417 29.829
OVERFLOW***: (000001) .00 .000 .000 .000
TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00
PEAK FLOW REDUCTION (Qout/Qin)(%)= 60.396
TIME SHIFT OF PEAK FLOW (min)= 143.00
-----
```

```

| CALIB STANDHYD | Area (ha)= 8.44
| 03:301 DT= 1.00 | Total Imp(h)= 60.00 Dir. Conn.(%)= 25.00

-----
IMPERVIOUS          PERVIOUS (I)
Surface Area (ha)= 5.06 3.38
Dep. Storage (cm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 700.00 35.00
Mannings n = .013 .250

Max.eff.Inten.(mm/hr)= 12.52 15.15
Storage Cover (min)= 12.00 21.00
Unit Hyd. Tpeak (min)= 11.70 (ii) 21.48 (iii)
Unit Hyd. Tpeak (min)= 12.00 21.00
Unit Hyd. Tpeak (cms)= .10 .05

PEAK FLOW (cms)= .07 .13 *TOTALS*
TIME TO PEAK (hrs)= 2.00 3.12 .003 (iii)
RUNOFF VOLUME (mm)= 58.99 33.98 40.243
TOTAL RAINFALL (mm)= 59.60 59.60 59.600
RUNOFF COEFFICIENT = .99 .57 .675

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN= 76.5 Ia= Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
    THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0116-----
*
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN:03 (301) |
| OUT:04 (POND) |

-----
OUTFLOW STORAGE | OUTFLOW STORAGE |
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .059 .3300E+00
.007 .3000E+01 | .062 .3600E+00
.009 .6000E+01 | .065 .3900E+00
.011 .9000E+01 | .068 .4200E+00
.026 .1200E+02 | .070 .4500E+00
.033 .1500E+02 | .073 .4800E+00
.039 .1800E+02 | .075 .5100E+00
.043 .2100E+02 | .077 .5400E+00
.048 .2400E+02 | .529 .5700E+00
.052 .2700E+02 | .000 .0000E+00
.055 .3000E+02 | .000 .0000E+00

ROUTING RESULTS      AREA      QPEAK      TPEAK      R.V.
-----
INFLOW >03 (301) | 8.44 .203 3.050 40.243
OUTFLOW<04 (POND) | 8.44 .050 6.650 40.242
OVERFLOW<+ (00001) | .00 .000 .000 .000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/ Qin] (%)= 24.613
TIME SHIFT OF PEAK FLOW (min)= 216.00
MAXIMUM STORAGE USED (ha.m.)=.2580E+00

-----
001:0117-----
*
* Area 401

| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.136
PEAK FLOW (cms)= .163 (I)
TIME TO PEAK (hrs)= 5.067
RUNOFF VOLUME (mm)= 20.152
TOTAL RAINFALL (mm)= 59.600
RUNOFF COEFFICIENT = .338

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0118-----
*
* Area 501

| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(h)= 65.00 Dir. Conn.(%)= 35.00

```

Surface Area (ha)= 2.55 1.37
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 500.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 12.52 14.99
over (min)= 10.00 19.00
Storage Coeff. (min)= 9.56 (ii) 19.38 (ii)
Unit Hyd. Tpeak (min)= 10.00 19.00
Unit Hyd. peak (cms)= .12 .06
TOTALS
PEAK FLOW (cms)= .05 .05 .099 (iii)
TIME TO PEAK (hrs)= 2.00 3.10 3.017
RUNOFF VOLUME (mm)= 59.00 33.84 42.648
TOTAL RAINFALL (mm)= 59.60 59.60 59.600
RUNOFF COEFFICIENT = .99 .57 .716
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0119-----
*
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>06:(S01) |
| OUT<07:(POND) |
***** OUTFLOW STORAGE TABLE *****
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .074 .1200E+00
.004 .1500E-01 | .080 .1350E+00
.005 .3000E-01 | .086 .1500E+00
.006 .4500E-01 | .092 .1650E+00
.036 .6000E-01 | .098 .1800E+00
.048 .7500E-01 | .325 .1950E+00
.058 .9000E-01 | .735 .2100E+00
.066 .1050E+00 | .000 .0000E+00
ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >06: (S01) 3.92 .099 3.017 42.648
OUTFLOW <07: (POND) 3.92 .057 5.400 42.648
OVERFLOW <<: (000001) .00 .000 .000 .000
TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00
PEAK FLOW REDUCTION [Qout/Qin](%)= 57.722
TIME SHIFT OF PEAK FLOW (min)= 143.00
MAXIMUM STORAGE USED (ha.m.)=.8876E-01

001:0120-----
*
*
* 10 year - 12hr AES
*
*
| READ STORM | Filename: C:\SWMHYM-1\LAKEST-1\10AES12.atm
| Ptotal= 69.30 mm | Comments: 10 year AES 12hr

TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
1.00 12.474 | 4.00 10.395 | 7.00 2.079 | 10.00 .000
2.00 14.553 | 5.00 9.702 | 8.00 .693 | 11.00 .000
3.00 13.860 | 6.00 5.544 | 9.00 .000 | 12.00 .000

001:0121-----
*
* Area 101
*
| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .14 .14
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.90 2.90
Length (m)= 42.00 35.00
Mannings n = .013 .250

Max.eff.Inten.(mm/hr)= 14.55 12.84
over (min)= 2.00 16.00
Storage Coeff. (min)= 2.38 (ii) 15.63 (ii)
Unit Hyd. Tpeak (min)= 2.00 16.00
Unit Hyd. peak (cms)= .50 .07
TOTALS
PEAK FLOW (cms)= .00 .00 .009 (iii)
TIME TO PEAK (hrs)= 2.00 3.05 3.000
RUNOFF VOLUME (mm)= 68.70 41.17 50.805
TOTAL RAINFALL (mm)= 69.30 69.30 69.300
RUNOFF COEFFICIENT = .99 .59 .733
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0122-----
*
* Area 201
*
| CALIB STANDHYD | Area (ha)= .32
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .16 .16
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.80 2.80
Length (m)= 20.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 14.55 12.85
over (min)= 2.00 15.00
Storage Coeff. (min)= 1.54 (ii) 14.92 (ii)
Unit Hyd. Tpeak (min)= 2.00 15.00
Unit Hyd. peak (cms)= .65 .08
TOTALS
PEAK FLOW (cms)= .00 .01 .010 (iii)
TIME TO PEAK (hrs)= 2.00 3.05 3.000
RUNOFF VOLUME (mm)= 68.70 41.17 50.805
TOTAL RAINFALL (mm)= 69.30 69.30 69.300
RUNOFF COEFFICIENT = .99 .59 .733
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0123-----
*
* Area 301
*
| CALIB STANDHYD | Area (ha)= 8.44
| 03:301 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 25.00

IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 5.06 3.38
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 700.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 14.55 18.74
over (min)= 11.00 20.00
Storage Coeff. (min)= 11.02 (ii) 20.00 (ii)
Unit Hyd. Tpeak (min)= 11.00 20.00
Unit Hyd. peak (cms)= .10 .06
TOTALS
PEAK FLOW (cms)= .09 .17 .248 (iii)
TIME TO PEAK (hrs)= 2.00 3.08 3.033
RUNOFF VOLUME (mm)= 68.69 42.15 48.792
TOTAL RAINFALL (mm)= 69.30 69.30 69.300
RUNOFF COEFFICIENT = .99 .61 .704
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0124-----
*
*
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>03:(S01) |
| OUT<04:(POND) |
***** OUTFLOW STORAGE TABLE *****
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)

```

.000 .0000E+00 | .059 .3300E+00
.007 .3000E-01 | .062 .3600E+00
.009 .6000E-01 | .065 .3900E+00
.011 .9000E-01 | .068 .4200E+00
.026 .1200E+00 | .070 .4500E+00
.033 .1500E+00 | .073 .4800E+00
.039 .1800E+00 | .075 .5100E+00
.043 .2100E+00 | .077 .5400E+00
.048 .2400E+00 | .529 .5700E+00
.052 .2700E+00 | .000 .0000E+00
.055 .3000E+00 | .000 .0000E+00

ROUTING RESULTS      AREA      QPEAK      TPEAK      R.V.
-----
INFLOW >03: (301 )  8.44      .248      3.033      48.792
OUTFLOW<04: (POND ) 8.44      .057      6.667      48.790
OVERFLOW***: (000001) .00      .000      .000      .000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin] (%)= 22.966
TIME SHIFT OF PEAK FLOW (min)= 218.00
MAXIMUM STORAGE USED (ha.m.)=-.3159E+00

-----
001:0125-----
*
* Area 401
*
-----
| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:101 DT= 2.00 | Ia 4.000 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .450
|
Unit Hyd Qpeak (cms)= 1.136

PEAK FLOW (cms)= .211 (i)
TIME TO PEAK (hrs)= 3.267
RUNOFF VOLUME (mm)= 26.144
TOTAL RAINFALL (mm)= 69.300
RUNOFF COEFFICIENT = .377

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0126-----
*
* Area 501
*
-----
| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 35.00
|
|
| IMPERVIOUS PERVIOUS (i)
| Surface Area (ha)= 2.55 1.37
| Dep. Storage (mm)= .60 2.50
| Average Slope (%)= 4.90 6.40
| Length (m)= 500.00 35.00
| Mannings n = .013 .250
|
| Max.eff.Inten.(mm/hr)= 14.55 18.54
| over (min)= 9.00 18.00
| Storage Coeff. (min)= 9.00 (ii) 18.02 (ii)
| Unit Hyd. Tpeak (min)= 9.00 18.00
| Unit Hyd. peak (cms)= .13 .06
|
| *TOTALS*
| PEAK FLOW (cms)= .06 .07 .120 (iii)
| TIME TO PEAK (hrs)= 2.00 3.07 3.017
| RUNOFF VOLUME (mm)= 68.70 41.99 51.340
| TOTAL RAINFALL (mm)= 69.30 69.30 69.300
| RUNOFF COEFFICIENT = .99 .61 .741
|
| (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
| CN* = 76.5 Ia = Dep. Storage (Above)
| (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
| THAN THE STORAGE COEFFICIENT.
| (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0127-----
*
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>06: (501 ) |
| OUT<07: (POND ) |
|-----
| OUTFLOW STORAGE | OUTFLOW STORAGE
| (cms) (ha.m.) | (cms) (ha.m.)
| .000 .0000E+00 | .074 .1200E+00
| .004 .1500E-01 | .080 .1350E+00
| .005 .3000E-01 | .086 .1500E+00
| .006 .4500E-01 | .092 .1650E+00
| .036 .6000E-01 | .098 .1800E+00
|-----
```

```

.048 .7500E-01 | .325 .1950E+00
.058 .9000E-01 | .735 .2100E+00
.066 .1050E+00 | .000 .0000E+00

ROUTING RESULTS      AREA      QPEAK      TPEAK      R.V.
-----
INFLOW >06: (501 )  3.92      .120      3.017      51.340
OUTFLOW<07: (POND ) 3.92      .067      5.400      51.338
OVERFLOW***: (000001) .00      .000      .000      .000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin] (%)= 55.534
TIME SHIFT OF PEAK FLOW (min)= 143.00
MAXIMUM STORAGE USED (ha.m.)=-.1056E+00

-----
001:0128-----
*
*
*
*
* 25 year - 12hr AES
*
-----
| READ STORM | | Filename: C:\SWHYM-1\LANEST-1\25AES12.stm
| Ptotal= 81.30 mm | Comments: 25 year AES 12hr
|
| TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
| hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
| 1.00 14.634 | 4.00 12.195 | 7.00 2.439 | 10.00 .000
| 2.00 17.073 | 5.00 11.382 | 8.00 .813 | 11.00 .000
| 3.00 16.260 | 6.00 6.504 | 9.00 .000 | 12.00 .000
|-----
001:0129-----
*
* Area 101
*
-----
| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
|
|
| IMPERVIOUS PERVIOUS (i)
| Surface Area (ha)= .14 .14
| Dep. Storage (mm)= .60 2.50
| Average Slope (%)= 2.90 2.90
| Length (m)= 42.00 35.00
| Mannings n = .013 .250
|
| Max.eff.Inten.(mm/hr)= 17.07 16.00
| over (min)= 2.00 14.00
| Storage Coeff. (min)= 2.24 (ii) 14.36 (ii)
| Unit Hyd. Tpeak (min)= 2.00 14.00
| Unit Hyd. peak (cms)= .52 .08
|
| PEAK FLOW (cms)= .00 .01 *TOTALS*
| TIME TO PEAK (hrs)= 1.85 3.03 .010 (iii)
| RUNOFF VOLUME (mm)= 80.70 51.53 61.741
| TOTAL RAINFALL (mm)= 81.30 81.30 81.300
| RUNOFF COEFFICIENT = .99 .63 .759
|
| (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
| CN* = 82.0 Ia = Dep. Storage (Above)
| (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
| THAN THE STORAGE COEFFICIENT.
| (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----
001:0130-----
*
* Area 201
*
-----
| CALIB STANDHYD | Area (ha)= .32
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
|
|
| IMPERVIOUS PERVIOUS (i)
| Surface Area (ha)= .16 .16
| Dep. Storage (mm)= .60 2.50
| Average Slope (%)= 2.80 2.80
| Length (m)= 20.00 35.00
| Mannings n = .013 .250
|
| Max.eff.Inten.(mm/hr)= 17.07 16.00
| over (min)= 1.00 14.00
| Storage Coeff. (min)= 1.45 (ii) 13.70 (ii)
| Unit Hyd. Tpeak (min)= 1.00 14.00
| Unit Hyd. peak (cms)= .85 .08
|-----
```

.759

(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY

(111) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 21.284
TIME SHIFT OF PEAK FLOW (min)= 221.00
MAXIMUM STORAGE USED (ha.m.)=.3908E+00

```

Unit Hyd Qpeak (cms) = 1.136

(111) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY

```

PEAK FLOW REDUCTION [Qout/Qin] (%) = 52.946
TIME SHIFT OF PEAK FLOW (min) = 145.00
MAXIMUM STORAGE USED (ha.m.) = 1.1285E+00

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
1.00	16.272	4.00	13.560	7.00	2.712	10.00	.000
2.00	18.984	5.00	12.656	8.00	.904	11.00	.000
3.00	18.080	6.00	7.232	9.00	.000	12.00	.000

```

-----
001:0137-----
*
*
* Area 101
*
-----
| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .14 .14
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.90 2.90
Length (m)= 42.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 18.98 18.41
over (min)= 2.00 14.00
Storage Coeff. (min)= 2.14 (ii) 13.61 (ii)
Unit Hyd. Tpeak (min)= 2.00 14.00
Unit Hyd. peak (cms)= .53 .08
*TOTALS*
PEAK FLOW (cms)= .01 .01 .012 (iii)
TIME TO PEAK (hrs)= 1.42 3.03 3.000
RUNOFF VOLUME (mm)= 89.80 59.59 70.164
TOTAL RAINFALL (mm)= 90.40 90.40 90.400
RUNOFF COEFFICIENT = .99 .66 .776
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
001:0138-----
*
* Area 201
*
-----
| CALIB STANDHYD | Area (ha)= .32
| 02:201 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= .16 .16
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 2.80 2.80
Length (m)= 20.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 18.98 18.43
over (min)= 1.00 13.00
Storage Coeff. (min)= 1.39 (ii) 12.97 (ii)
Unit Hyd. Tpeak (min)= 1.00 13.00
Unit Hyd. peak (cms)= .87 .09
*TOTALS*
PEAK FLOW (cms)= .01 .01 .014 (iii)
TIME TO PEAK (hrs)= 1.28 3.03 3.000
RUNOFF VOLUME (mm)= 89.80 59.59 70.164
TOTAL RAINFALL (mm)= 90.40 90.40 90.400
RUNOFF COEFFICIENT = .99 .66 .776
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
001:0139-----
*
* Area 301
*
-----
| CALIB STANDHYD | Area (ha)= 8.44
| 03:301 DT= 1.00 | Total Imp(%)= 60.00 Dir. Conn.(%)= 25.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 5.06 3.38
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 700.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 18.98 26.79
over (min)= 10.00 18.00
Storage Coeff. (min)= 9.91 (ii) 17.69 (ii)
Unit Hyd. Tpeak (min)= 10.00 18.00
Unit Hyd. peak (cms)= .11 .06
*TOTALS*
PEAK FLOW (cms)= .11 .24 .348 (iii)
TIME TO PEAK (hrs)= 2.00 3.05 3.017
RUNOFF VOLUME (mm)= 89.79 60.69 67.978
TOTAL RAINFALL (mm)= 90.40 90.40 90.400

```

```

RUNOFF COEFFICIENT = .99 .67 .752
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
001:0140-----
*
* ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>03:(301 ) |
| OUT<04:(POND ) |
-----
OUTFLOW STORAGE | OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .059 .3300E+00
.007 .3000E+01 | .062 .3600E+00
.009 .6000E+01 | .065 .3900E+00
.011 .9000E+01 | .068 .4200E+00
.026 .1200E+00 | .070 .4500E+00
.033 .1500E+00 | .073 .4800E+00
.039 .1800E+00 | .075 .5100E+00
.043 .2100E+00 | .077 .5400E+00
.048 .2400E+00 | .529 .5700E+00
.052 .2700E+00 | .000 .0000E+00
.055 .3000E+00 | .000 .0000E+00
ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >03:(301 ) 8.44 .348 3.017 67.978
OUTFLOW <04:(POND ) 8.44 .070 6.733 67.977
OVERFLOW<04:(000001) .00 .000 .000 .000
TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00
PEAK FLOW REDUCTION [Qout/Qin](%)= 20.192
TIME SHIFT OF PEAK FLOW (min)= 223.00
MAXIMUM STORAGE USED (ha.m.)= .4496E+00

```

```

-----
001:0141-----
*
* Area 401
*
-----
| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .450
-----
Unit Hyd Qpeak (cms)= 1.136
PEAK FLOW (cms)= .330 (i)
TIME TO PEAK (hrs)= 3.233
RUNOFF VOLUME (mm)= 40.526
TOTAL RAINFALL (mm)= 90.400
RUNOFF COEFFICIENT = .448
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
001:0142-----
*
* Area 501
*
-----
| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 35.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 2.55 1.37
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 500.00 35.00
Mannings n = .013 .250
Max.eff.Inten.(mm/hr)= 18.98 26.51
over (min)= 8.00 16.00
Storage Coeff. (min)= 8.10 (ii) 15.91 (ii)
Unit Hyd. Tpeak (min)= 8.00 16.00
Unit Hyd. peak (cms)= .14 .07
*TOTALS*
PEAK FLOW (cms)= .07 .10 .167 (iii)
TIME TO PEAK (hrs)= 2.00 3.03 3.000
RUNOFF VOLUME (mm)= 89.79 60.50 70.760
TOTAL RAINFALL (mm)= 90.40 90.40 90.400
RUNOFF COEFFICIENT = .99 .67 .783
(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL

```

* Area 201
*

CALIB STANDHYD		Area (ha)=	.32		
02:201 DT= 1.00		Total Imp(%)=	50.00	Dir. Conn.(%)=	35.00

	IMPERVIOUS	PERVIOUS (i)	
Surface Area (ha)	.16	.16	
Dep. Storage (mm)	.60	2.50	
Average Slope (%)	2.80	2.80	
Length (m)	20.00	35.00	
Mannings n	.013	.250	
Max. eff. Inten. (mm/hr)	20.94	20.93	
Time over (min)	1.00	12.90	
Storage Coeff. (min)	1.33 (ii)	12.34 (ii)	
Unit Hyd. Peak (min)	1.00	12.00	
Unit Hyd. Peak (cms)	.90	.09	
			TOTALS
PEAK FLOW (cms)	.01	.01	.015 (iii)
TIME TO PEAK (hrs)	1.28	3.02	3.00
RUNOFF VOLUME (mm)	99.10	67.96	78.862
TOTAL RAINFALL (mm)	99.70	99.70	99.700
RUNOFF COEFFICIENT	.99	.68	.791

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

*
* Area 301
*

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha) =	5.06	3.38
Dep. Storage (mm) =	.60	2.50
Average Slope (%) =	4.90	6.40
Length (m) =	700.00	35.00
Mannings n =	.013	.250
Max. eff. Inten. (mm/hr) =	20.94	30.40
over (min) =	10.00	17.00
Storage Coeff. (min) =	9.53 (ii)	16.93 (ii)
Unit Hyd. Peak (min) =	10.00	17.00
Unit Hyd. Peak (cms) =	.12	.07
		TOTALS
PEAK FLOW (cms) =	1.2	.28
TIME TO PEAK (hrs) =	2.00	3.93 (iii)
	12	3.05
RUNOFF VOLUME (mm) =	99.09	69.11
TIME TO RAINFALL (min) =	99.70	76.618
	99.70	99.700
RUNOFF COEFFICIENT =	.99	.69
		.768

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

[illegible]

ROUTING RESERVATION		Requested routing time step = 1.0 min.				
IN:03: (301)						
OUT:04: (POND)						
OUTFLOW	OUTFLOW STORAGE	OUTFLOW	OUTFLOW STORAGE	TABLE		
(cms)	(ft.m.m)	(cms)	(ft.m.m)			
.000	.0000E+00	.059	.3300E+00			
.007	.3000E+01	.062	.3600E+00			
.009	.6000E+01	.065	.3900E+00			
.011	.9000E+01	.068	.4200E+00			
.026	.1200E+00	.070	.4500E+00			
.033	.1500E+00	.073	.4800E+00			
.039	.1800E+00	.075	.5100E+00			
.043	.2100E+00	.077	.5400E+00			
.048	.2400E+00	.529	.5700E+00			
.052	.2700E+00	.000	.0000E+00			
.055	.3000E+00	.000	.0000E+00			
ROUTING RESULTS						
	AREA	PEAK	TPEAK	R.V.		
INFL: 8:30: (301)	.393	.44	76.6167	76.6167		
OUTFLOW:04: (POND)	8.44	.075	6.783	76.616		
OVERFLOW:*** (000001)	.00	.000	.000	.000		

TOTAL NUMBER OF SIMULATED OVERFLOWS =
CUMULATIVE TIME OF OVERFLOWS (hours) =
PERCENTAGE OF TIME OVERFLOWING (%) =

```

PEAK FLOW REDUCTION [Qout/Qin] (%) = 51.210
TIME SHIFT OF PEAK FLOW (min) = 146.00
MAXIMUM STORAGE USED (ha.m.) = .1471E+00

```

| CALIB ST.

03:301

* 100 year - 12hr AES

READ STORM		Filename: C:\SWMHYM-1\LAKEST-1\100AES12.stm	
Ptotal= 99.70 mm		Comments: 100 year AES 12hr	
TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr
1.00	17.946	4.00	14.955
2.00	20.937	5.00	13.958
3.00	19.940	6.00	7.976
		7.00	2.991
		8.00	.997
		9.00	.000
		10.00	11.00
		11.00	.000

TOTAL
RUNOFF

* Area 101

```

+-----+
| CALIB STANDHYD | Area (ha)= .28
| 01:101 DT= 1.00 | Total Imp(%)= 50.00 Dir. Conn.(%)= 35.00

```

	IMPERVIOUS	PERVIOUS (i)
Surface Area (ha) =	.14	.14
Dep. Storage (mm) =	.60	2.50
Average Slope (ft) =	2.90	2.90
Length (mi) =	42.00	35.00
Mannings n =	.013	.250
Max. eff. flow (mm/hr) =	20.94	20.92
over (min)	2.00	13.00
Storage Coeff. (min) =	2.06 (ii)	12.96 (ii)
Unit Hyd. Peak (min) =	2.00	13.00
Unit Hyd. Peak (cms) =	.55	.09
		TOTALS
PEAK FLOW (cms) =	.01	.013 (iii)
TIME TO PEAK (hrs) =	1.40	3.00
RUNOFF VOLUME (mm) =	99.10	78.862
SUM TOTAL RAINFALL (mm) =	99.70	99.700
RUNOFF COEFFICIENT =	.99	.791

- (i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 82.0 Ia = Dep. Storage (Above)
- (ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT.
- (iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

TOTAL NUMBER OF SIMULATED OVERFLOWS -
CUMULATIVE TIME OF OVERFLOWS (hours)-
PERCENTAGE OF TIME OVERFLOWING (%) -

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 19.066
TIME SHIFT OF PEAK FLOW (min)= 226.00
MAXIMUM STORAGE USED (ha.m.)=-.5113E+00
-----
001:0149-----
*
* Area 401
*
-----
| CALIB NASHYD | Area (ha)= 13.38 Curve Number (CN)=72.20
| 05:401 DT= 2.00 | Ia (mm)= 4.000 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .450

Unit Hyd Qpeak (cms)= 1.136

PEAK FLOW (cms)= .387 (i)
TIME TO PEAK (hrs)= 3.200
RUNOFF VOLUME (mm)= 47.331
TOTAL RAINFALL (mm)= 99.700
RUNOFF COEFFICIENT = .475

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0150-----
*
* Area 501
*
-----
| CALIB STANDHYD | Area (ha)= 3.92
| 06:501 DT= 1.00 | Total Imp(%)= 65.00 Dir. Conn.(%)= 35.00
-----
IMPERVIOUS PERVIOUS (i)
Surface Area (ha)= 2.55 1.37
Dep. Storage (mm)= .60 2.50
Average Slope (%)= 4.90 6.40
Length (m)= 500.00 35.00
Mannings n = .013 .250

Max. eff. Inten. (mm/hr)= 20.94 30.08
over (min) 8.00 15.00
Storage Coeff. (min)= 7.79 (ii) 15.22 (ii)
Unit Hyd. Tpeak (min)= 8.00 15.00
Unit Hyd. peak (cms)= .14 .07

*TOTALS*
PEAK FLOW (cms)= .08 .11 .187 (iii)
TIME TO PEAK (hrs)= 2.00 3.03
RUNOFF VOLUME (mm)= 99.10 68.91 79.480
TOTAL RAINFALL (mm)= 99.70 99.70 99.700
RUNOFF COEFFICIENT = .99 .69 .797

(i) CN PROCEDURE SELECTED FOR PERVIOUS LOSSES:
CN* = 76.5 Ia = Dep. Storage (Above)
(ii) TIME STEP (DT) SHOULD BE SMALLER OR EQUAL
THAN THE STORAGE COEFFICIENT*
(iii) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0151-----
*
-----
| ROUTE RESERVOIR | Requested routing time step = 1.0 min.
| IN>06:(501 ) |
| OUT<07:(POND ) |
-----
***** OUTFLOW STORAGE TABLE *****
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.) | (cms) (ha.m.)
.000 .0000E+00 | .074 .1200E+00
.004 .1500E-01 | .080 .1350E+00
.005 .3000E-01 | .086 .1500E+00
.006 .4500E-01 | .092 .1650E+00
.036 .6000E-01 | .098 .1800E+00
.048 .7500E-01 | .325 .1950E+00
.058 .9000E-01 | .735 .2100E+00
.066 .1050E+00 | .000 .0000E+00

ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >06: (501 ) 3.92 .187 3.000 79.480
OUTFLOW<07: (POND ) 3.92 .093 5.450 79.479
OVERFLOW***: (000001) .00 .000 .000 .000

TOTAL NUMBER OF SIMULATED OVERFLOWS = 0
CUMULATIVE TIME OF OVERFLOWS (hours)= .00
PERCENTAGE OF TIME OVERFLOWING (%)= .00

PEAK FLOW REDUCTION [Qout/Qin](%)= 49.629
TIME SHIFT OF PEAK FLOW (min)= 147.00
MAXIMUM STORAGE USED (ha.m.)=-.1669E+00
-----
001:0152-----

```

```

*
*
***** FINISH *****
***** WARNINGS / ERRORS / NOTES *****
001:0066 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0070 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0076 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0079 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0084 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0087 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0092 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0095 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0100 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
001:0103 COMPUTE VOLUME
*** WARNING: Calculated volume may not be the maximum.
Simulation ended on 2004-09-19 at 02:53:39
-----

```

Stage-Storage-Discharge Relationship **Pond 301**

Orifice 1 - quality

orifice	$Q=cA(2gh)^{0.5}$		
orifice diameter	0.1	c	0.6
orifice radius	0.05	g	9.81
orifice area	0.00785	2g	19.62

Orifice 2 - quantity

orifice	$Q=cA(2gh)^{0.5}$		
orifice diameter	0.14	c	0.6
orifice radius	0.07	g	9.81
orifice area	0.01539	2g	19.62

Overflow

overflow	$Q=CLH^{1.5}$
c	1.67
L	8.5

Description	Elevation	Storage (m3)	ha m	Orifice 1		Orifice 2		Overflow		Qt
				Head (m)	Discharge (m3/s)	Head (m)	Discharge (m3/s)			
		0	0.0000	0	0.0000					0.0000
		300.0	0.0300	0.10	0.0066					0.0066
		600.0	0.0600	0.20	0.0093					0.0093
Top of quality		900.0	0.0900	0.30	0.0114	0	0			0.0114
		1200.0	0.1200	0.40	0.0132	0.1000	0.0129			0.0261
		1500.0	0.1500	0.50	0.0148	0.2000	0.0183			0.0330
		1800.0	0.1800	0.60	0.0162	0.3000	0.0224			0.0386
		2100.0	0.2100	0.7000	0.0175	0.4000	0.0259			0.0433
		2400.0	0.2400	0.8000	0.0187	0.5000	0.0289			0.0476
		2700.0	0.2700	0.9000	0.0198	0.6000	0.0317			0.0515
		3000.0	0.3000	1.0000	0.0209	0.7000	0.0342			0.0551
		3300.0	0.3300	1.1000	0.0219	0.8000	0.0366			0.0585
		3600.0	0.3600	1.2000	0.0229	0.9000	0.0388			0.0616
		3900.0	0.3900	1.3000	0.0238	1.0000	0.0409			0.0647
		4200.0	0.4200	1.4000	0.0247	1.1000	0.0429			0.0676
		4500.0	0.4500	1.5000	0.0256	1.2000	0.0448			0.0703
		4800.0	0.4800	1.6000	0.0264	1.3000	0.0466			0.0730
		5100.0	0.5100	1.6000	0.0264	1.4000	0.0484			0.0748
top of quantity		5400.0	0.5400	1.7000	0.0272	1.5000	0.0501	0.0000	0.0000	0.0773
		5700.0	0.5700	1.8000	0.0280	1.6000	0.0517	0.1000	0.4489	0.5286
		6000.0	0.6000	1.9000	0.0288	1.7000	0.0533	0.2000	1.2696	1.3517
top of overflow		6300.0	0.6300	2.0000	0.0295	1.8000	0.0549	0.3000	2.3325	2.4168

Stage-Storage-Discharge Relationship Pond 501

Orifice 1 - quality

orifice	$Q=cA(2gh)^{0.5}$		
orifice diameter	0.075	c	0.6
orifice radius	0.0375	g	9.81
orifice area	0.00442	2g	19.62

Orifice 2 - quantity

orifice	$Q=cA(2gh)^{0.5}$		
orifice diameter	0.207	c	0.6
orifice radius	0.1035	g	9.81
orifice area	0.03364	2g	19.62

Overflow

overflow	$Q=CLH^{1.5}$
c	1.67
L	4.2

Description	Elevation	Storage (m3)	ha m	Orifice 1		Orifice 2		Overflow		Qt
				Head (m)	Discharge (m3/s)	Head (m)	Discharge (m3/s)			
		0	0.0000	0	0.0000					0.0000
		150.0	0.0150	0.10	0.0037					0.0037
		300.0	0.0300	0.20	0.0052					0.0052
Top of quality		450.0	0.0450	0.30	0.0064	0	0			0.0064
		600.0	0.0600	0.40	0.0074	0.1000	0.0283			0.0357
		750.0	0.0750	0.50	0.0083	0.2000	0.0400			0.0483
		900.0	0.0900	0.60	0.0091	0.3000	0.0490			0.0581
		1050.0	0.1050	0.70	0.0098	0.4000	0.0565			0.0664
		1200.0	0.1200	0.80	0.0105	0.5000	0.0632			0.0737
		1350.0	0.1350	0.90	0.0111	0.6000	0.0692			0.0804
		1500.0	0.1500	1.00	0.0117	0.7000	0.0748			0.0865
		1650.0	0.1650	1.10	0.0123	0.8000	0.0800			0.0923
top of quantity		1800.0	0.1800	1.20	0.0129	0.9000	0.0848	0.0000	0.0000	0.0977
		1950.0	0.1950	1.30	0.0134	1.0000	0.0894	0.1000	0.2218	0.3246
		2100.0	0.2100	1.40	0.0139	1.1000	0.0938	0.2000	0.6274	0.7350
top of overflow		2250.0	0.2250	1.50	0.0144	1.2000	0.0979	0.3000	1.1525	1.2648

Pond 301

24 hour Draw Down

Event	25 mm	
volume	1058	m^3
24 hr avg	0.0122	m^3/s

Forebay Sizing Calculations

Settling Calculation

$$D = \text{SQRT}(rQ_p/V_s)$$

r	2	
Qp	0.0122	m^3/s
Vs	0.0003	m^3/s
D	9.04	m

Dispersion Calculation

$$D = 8Q/dV_f$$

Q	0.203	m^3/s
d	1	m
Vf	0.5	m/s
D	3.25	m

Width Calculation

$$W = D/8$$

D	9.04	m
W	1.13	m

Note:

Qp = discharge of quality event for 24 hr draw down

Q = Q 5 from SWMHYMO model

Pond 501

24 hour Draw Down

Event	25 mm	
volume	552	m^3
24 hr avg	0.0064	m^3/s

Forebay Sizing Calculations

Settling Calculation

$$D = \text{SQRT}(rQ_p/V_s)$$

r	2	
Qp	0.0064	m^3/s
Vs	0.0003	m^3/s
D	6.53	m

Dispersion Calculation

$$D = 8Q/dV_f$$

Q	0.099	m^3/s
d	1	m
Vf	0.5	m/s
D	1.58	m

Width Calculation

$$W = D/8$$

D	6.53	m
W	0.82	m

Note:

Qp = discharge of quality event for 24 hr draw down

Q = Q 5 from SWMHYMO model

Sediment Accumulation Pond 301

Initial Volume Available in Main Pond	1000	cubic metres	
Initial Volume Available in Forebay	500	cubic metres	
Target Volume for Cleanout	75 % remaining		
Contributing Area	8.44	ha	
Annual Loading @ 55%	1.9	cubic metres/ha	per MOE Table 6.3
annual accumulation (site)	16.036	cubic metres	

Main Pond 20 % of sediment

Year	Volume Available	Accumulated Sediment	% Volume Remaining
0	1000	0	100
1	996.8	3.2	100
2	993.6	6.4	99
3	990.4	9.6	99
4	987.2	12.8	99
5	984.0	16.0	98
6	980.8	19.2	98
7	977.5	22.5	98
8	974.3	25.7	97
9	971.1	28.9	97
10	967.9	32.1	97
11	964.7	35.3	96
12	961.5	38.5	96
13	958.3	41.7	96
14	955.1	44.9	96
15	951.9	48.1	95
16	948.7	51.3	95
17	945.5	54.5	95
18	942.3	57.7	94
19	939.1	60.9	94
20	935.9	64.1	94

Forebay 80 % of sediment

Year	Volume Available	Accumulated Sediment	% Volume Remaining
0	500	0	100
1	487.2	12.8	97
2	474.3	25.7	95
3	461.5	38.5	92
4	448.7	51.3	90
5	435.9	64.1	87
6	423.0	77.0	85
7	410.2	89.8	82
8	397.4	102.6	79
9	384.5	115.5	77
10	371.7	128.3	74
11	358.9	141.1	72
12	346.1	153.9	69
13	333.2	166.8	67
14	320.4	179.6	64
15	307.6	192.4	62
16	294.7	205.3	59
17	281.9	218.1	56

Sediment Accumulation Pond 501

Initial Volume Available in Main Pond	500	cubic metres	
Initial Volume Available in Forebay	300	cubic metres	
Target Volume for Cleanout	75 % remaining		
Contributing Area	3.92	ha	
Annual Loading @ 65%	2.5	cubic metres/ha	per MOE Table 6.3
annual accumulation (site)	9.8	cubic metres	

Main Pond 20 % of sediment

Year	Volume Available	Accumulated Sediment	% Volume Remaining
0	500	0	100
1	498.0	2.0	100
2	496.1	3.9	99
3	494.1	5.9	99
4	492.2	7.8	98
5	490.2	9.8	98
6	488.2	11.8	98
7	486.3	13.7	97
8	484.3	15.7	97
9	482.4	17.6	96
10	480.4	19.6	96
11	478.4	21.6	96
12	476.5	23.5	95
13	474.5	25.5	95
14	472.6	27.4	95
15	470.6	29.4	94
16	468.6	31.4	94
17	466.7	33.3	93
18	464.7	35.3	93
19	462.8	37.2	93
20	460.8	39.2	92

Forebay 80 % of sediment

Year	Volume Available	Accumulated Sediment	% Volume Remaining
0	300	0	100
1	292.2	7.8	97
2	284.3	15.7	95
3	276.5	23.5	92
4	268.6	31.4	90
5	260.8	39.2	87
6	253.0	47.0	84
7	245.1	54.9	82
8	237.3	62.7	79
9	229.4	70.6	76
10	221.6	78.4	74
11	213.8	86.2	71
12	205.9	94.1	69
13	198.1	101.9	66
14	190.2	109.8	63
15	182.4	117.6	61
16	174.6	125.4	58
17	166.7	133.3	56